

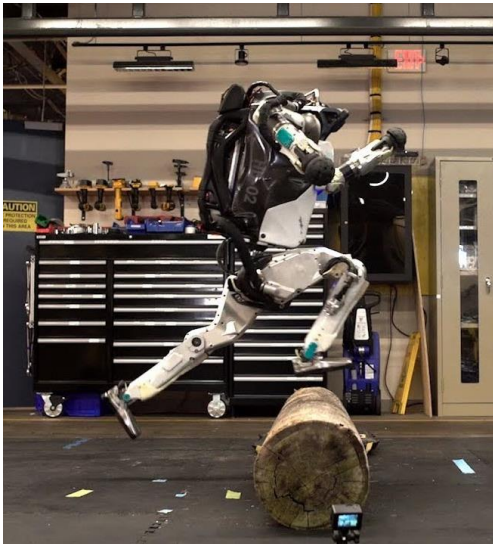
Computational Design Synthesis of Passive Dynamic Systems

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Robotic Systems

Active Robotic Systems

- Actuators and feedback control
- High task flexibility possible
- Responsive to environment
- High robustness



<https://www.bostondynamics.com/atlas>

Passive Robotic Systems

- No actuators and control
- No energy source necessary
- Potential to save energy and components



Passive dynamic walking, McGeer, T., 1990, International Journal of Robotics Research

Automated Topological Synthesis in Robotics

Active Dynamic Systems

- Evolving topology and control together

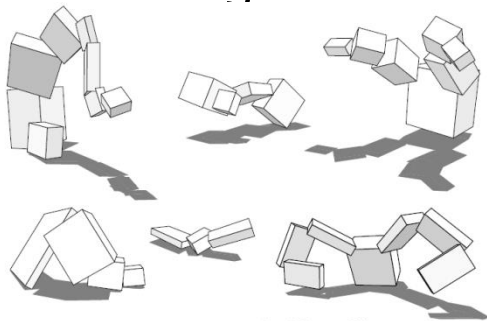
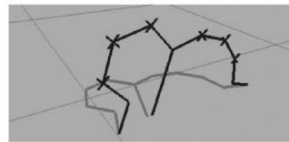


Figure 7: Creatures evolved for walking.
Evolving Virtual Creatures, Karl Sims, 1994

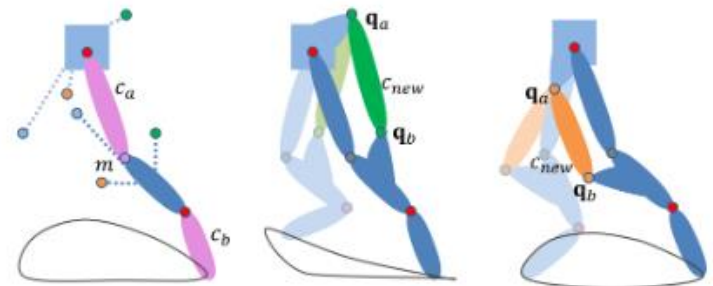


(c)

Generative Representations for the Automated Design
of Modular Physical Robots, G.Hornby, H.Lipson, 2003

Kinematic Systems

- Not considering causes of motion (forces, masses, ... do not matter)

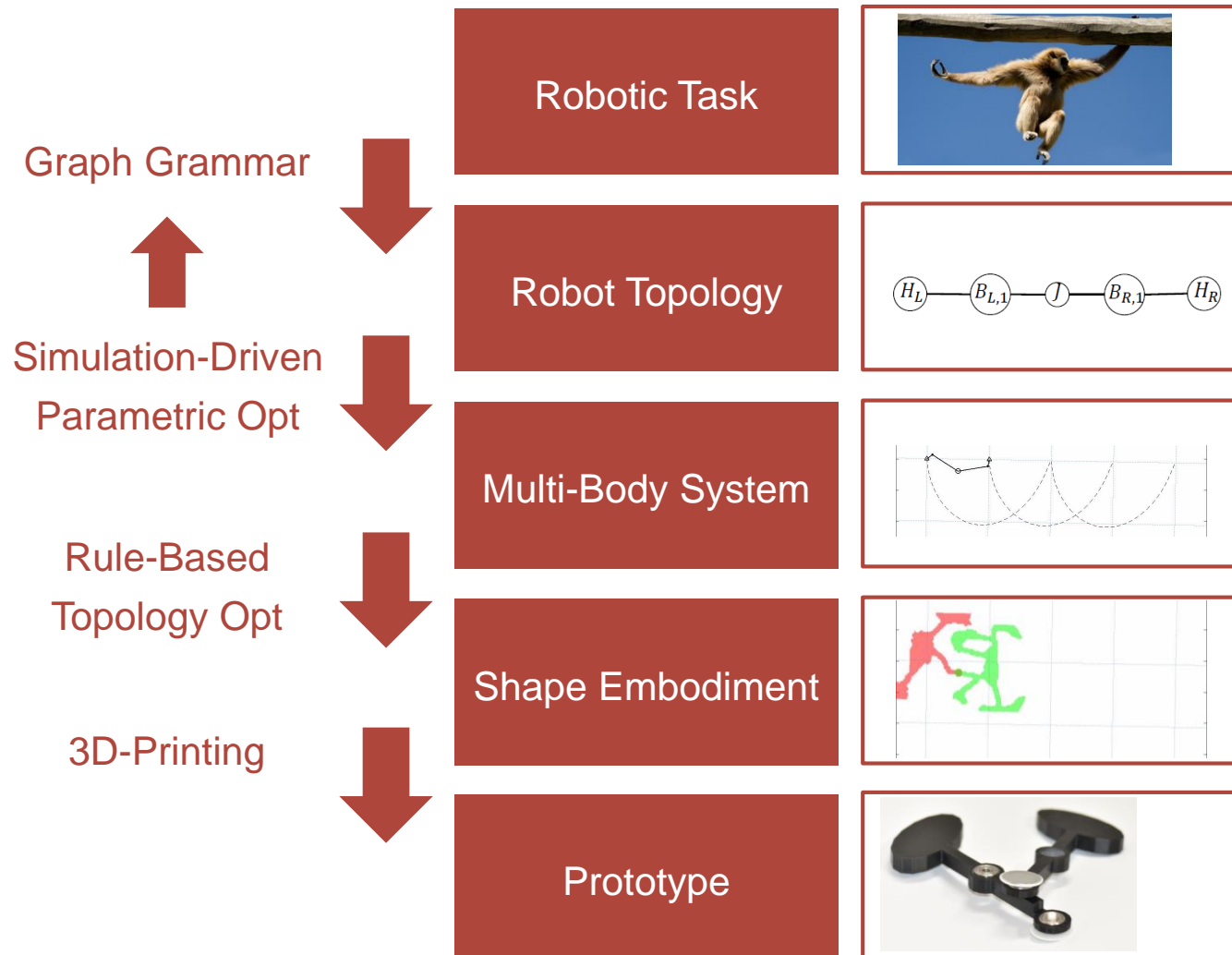


Computational Design of Linkage-Based Characters, Bernhard
Thomaszewski, Stelian Coros, Damien Gauge, Vittorio Megaro,
Eitan Grinspun, Markus Gross

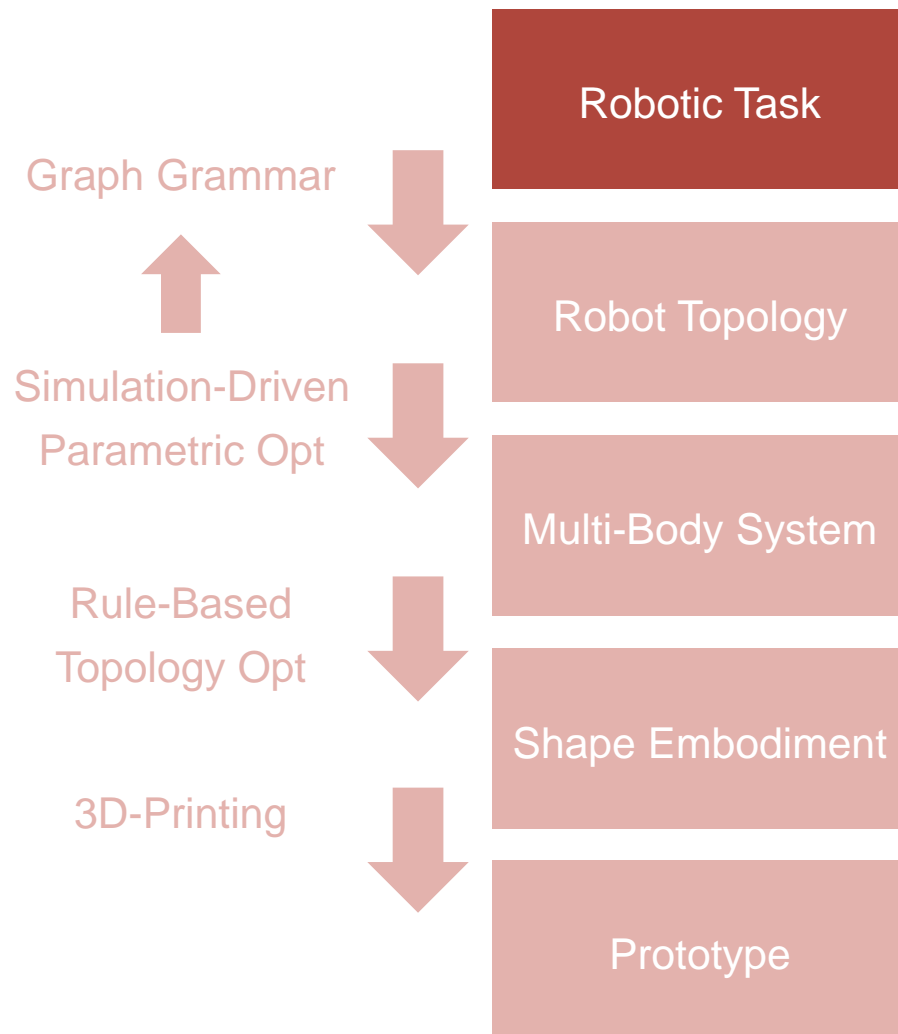
This Research: Passive Dynamic Systems

- Forces, masses, ... are important
- Do not draw energy from a source
- No feedback control

CDS of Passive Dynamic Systems - Overview



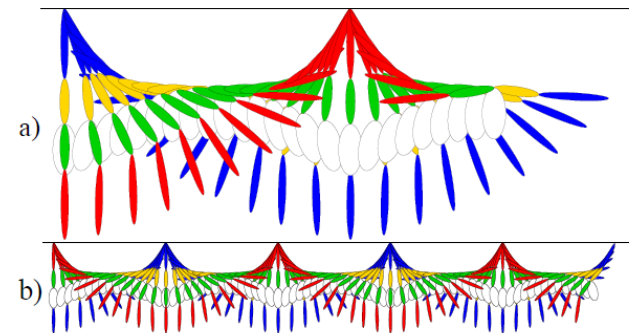
Example Problem: Brachiating



- Brachiating: The swinging locomotion of primates moving from one tree branch to the next.

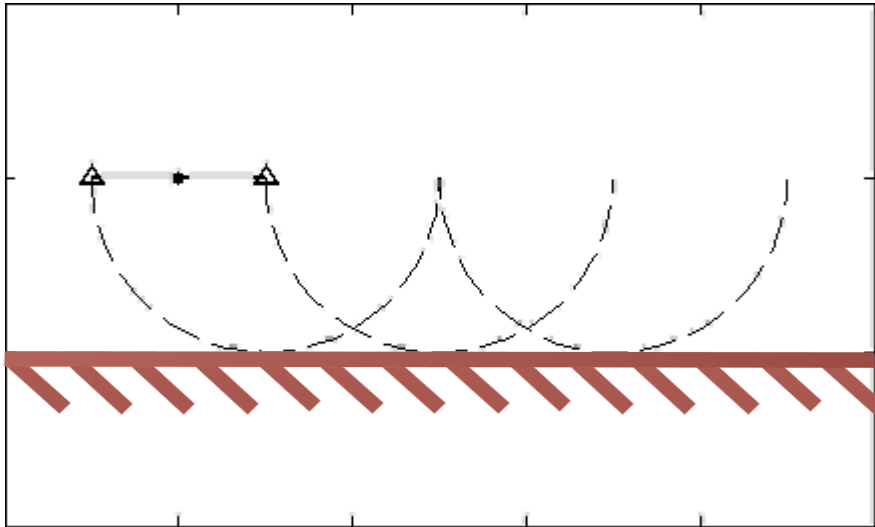


- Complex, bio-inspired models of passive dynamic brachiating exist:



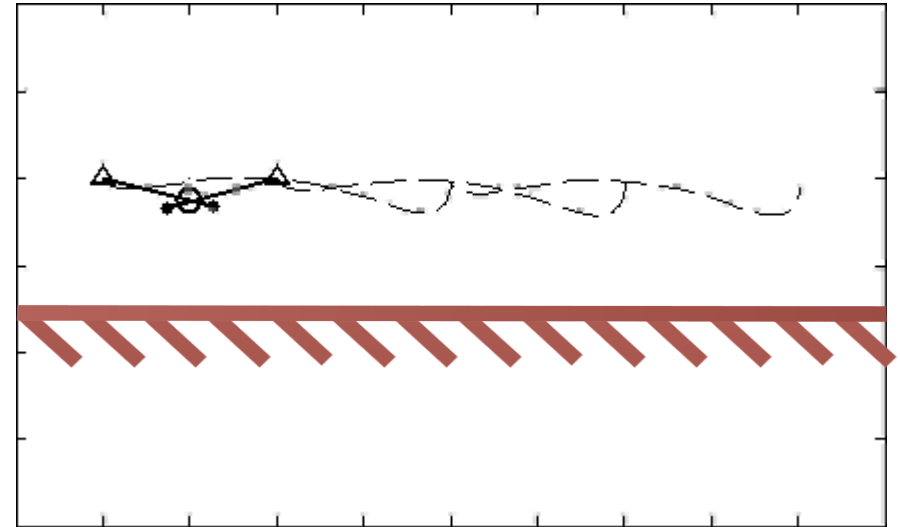
A five-link 2D brachiating ape model with life-like zero energy-cost motions, Mario Gomes, Andi L. Ruina, 2005

Motivation for Complex Brachiating Topologies



Single Pendulum

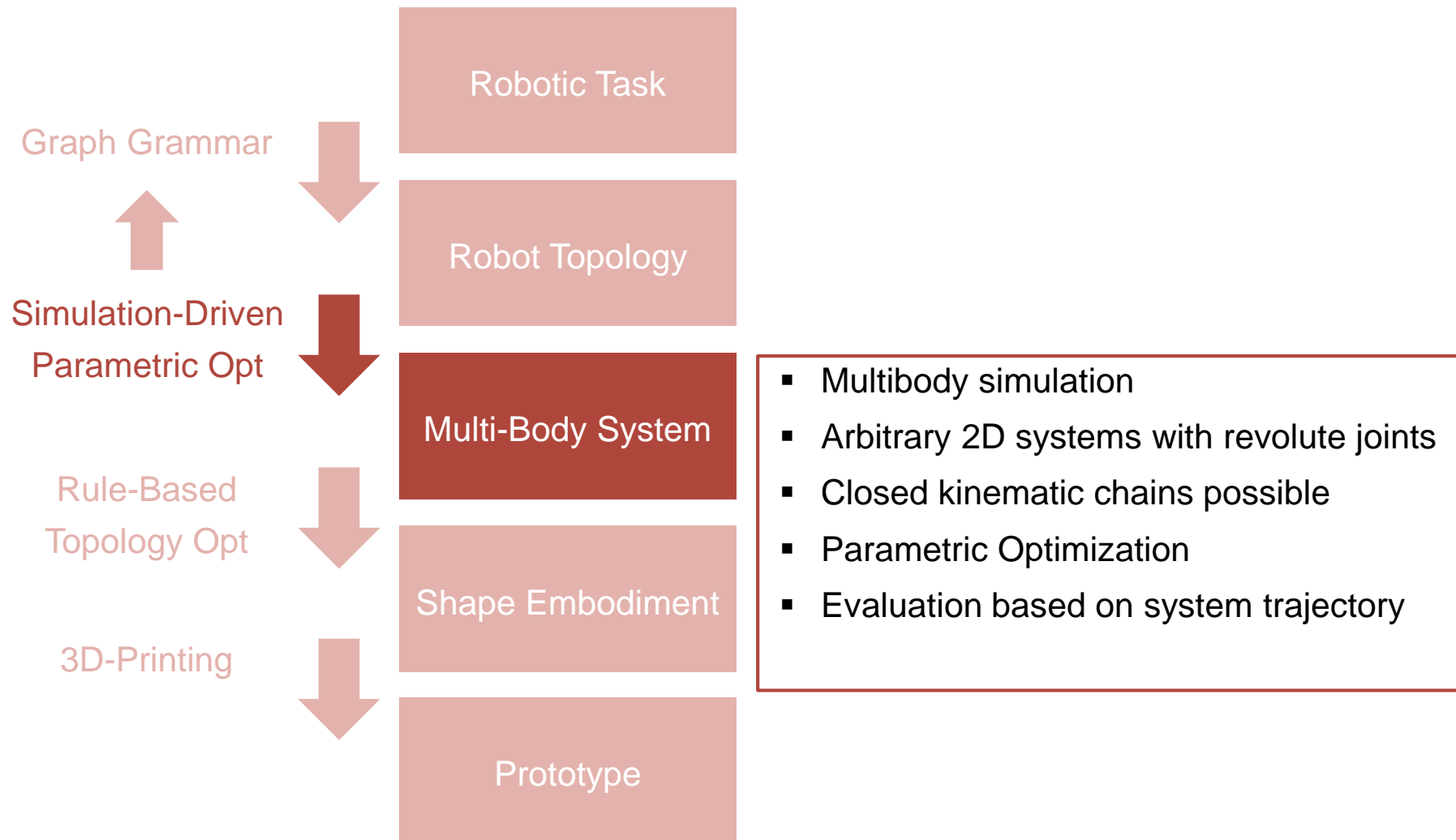
- Simplest possible solution



More Complex Solutions

- Might require less space
- Test for synthesis method

Simulation-Driven Parametric Optimization



Multi-Body Dynamics

Equations of motion
(set of ODEs)

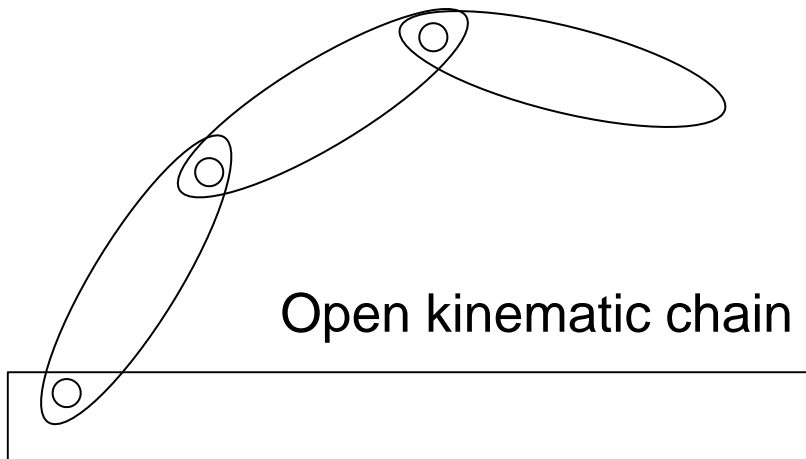
$$M(q, t)\ddot{q} - h(q, \dot{q}, t) = 0$$

M Mass matrix

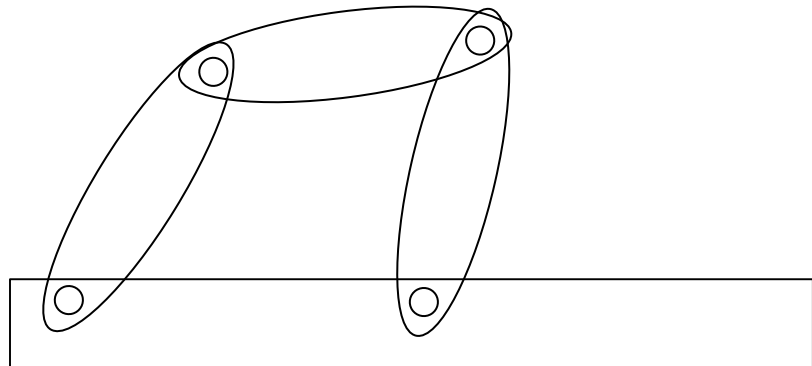
q System coordinates

h Forces (gravity, springs, ...)

Motion trajectories can be calculated using numeric integration.
Formulation works for open kinematic chains only.



Closed kinematic chain



Multi-Body Dynamics with Closed Kinematic Chains

Equations of motion for systems with closed kinematic chains
(Differential-Algebraic System)

$$M(q, t)\ddot{q} - h(q, \dot{q}, t) - W(q, t)\lambda = 0 \quad \text{Set of ODEs}$$

$$g(q, t) = 0 \quad \text{Set of algebraic Equations}$$

g Vector of Constraints (Same as \mathbf{C} in Lecture 3
“Kinematics of Mechanisms”)

λ Vector of constraining forces

$$W(q, t) = \frac{\partial g(q, t)}{\partial q} \quad \text{Matrix of generalized force directions (How constraining forces act on system coordinates)}$$

Multi-Body Dynamics with Closed Kinematic Chains

Transform into set of ODEs by taking second derivative of g

$$\left. \begin{aligned} M(q, t)\ddot{q} - h(q, \dot{q}, t) - W(q, t)\lambda &= 0 \\ \ddot{g}(q, t) = W^T(q, t)\ddot{q} + \zeta(q, \dot{q}, t) &= 0 \end{aligned} \right\}$$

Initial concitions: $\left\{ \begin{aligned} g(q_0, t_0) &= 0 \\ \dot{g}(q_0, \dot{q}_0, t_0) &= 0 \end{aligned} \right.$

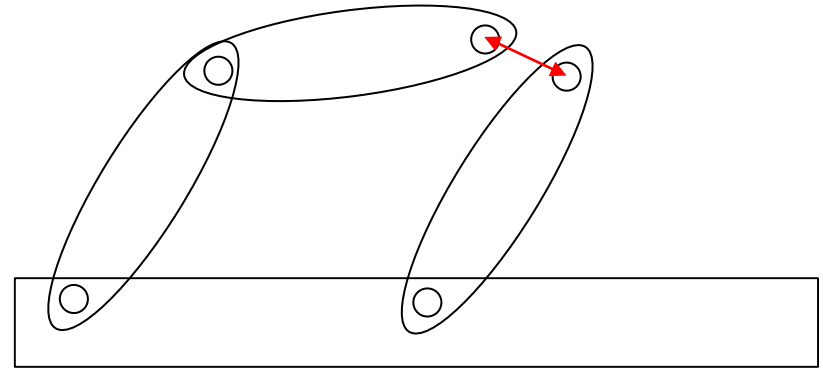
$$\lambda = -(W^T M^{-1} W)^{-1} (W^T M^{-1} h + \zeta)$$

Solve for λ
and \ddot{q}

$$\boxed{\begin{aligned} \ddot{q} &= M^{-1}(h + W\lambda) \\ g(q_0, t_0) &= 0 \\ \dot{g}(q_0, \dot{q}_0, t_0) &= 0 \end{aligned}}$$

Numerical problems and Stabilization

$$\begin{aligned}\ddot{q} &= M^{-1}(h + W\lambda) \\ g(q_0, t_0) &= 0 \\ \dot{g}(q_0, \dot{q}_0, t_0) &= 0\end{aligned}$$



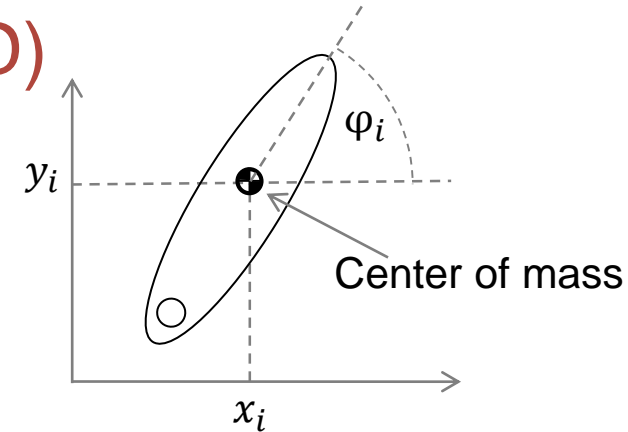
Numeric errors during integration can accumulate and break constraints

Baumgarte Stabilization:

Correct these errors during integration by replacing $\ddot{g} = 0$ by $\ddot{g} + 2\gamma\dot{g} + \gamma^2g = 0$ (change ζ accordingly)

Body Coordinate Representation (2D)

For each body i global coordinates x_i, y_i, φ_i
mass m_i and moment of inertia I_i



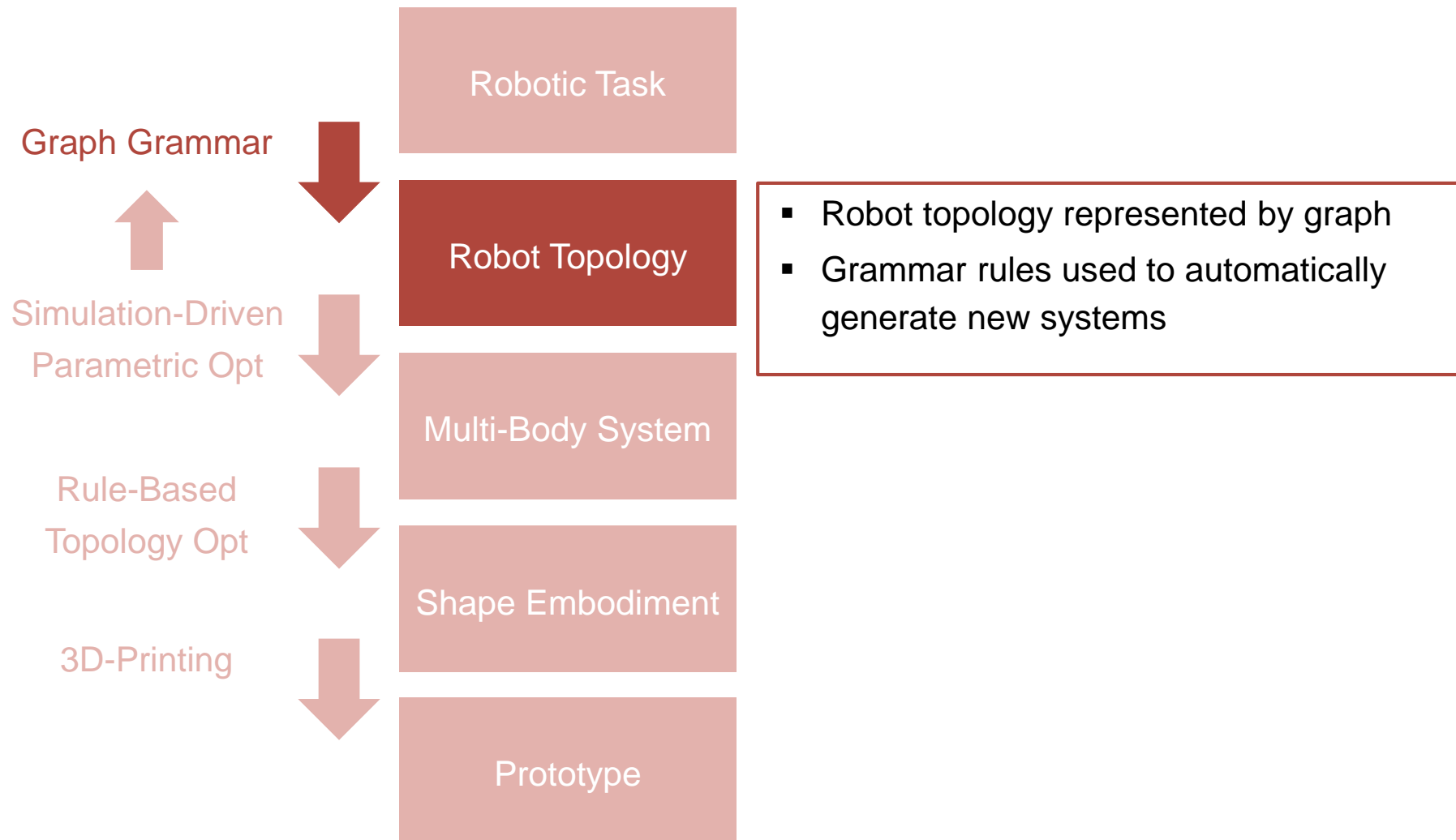
System coordinates: $\mathbf{q} = (x_1, y_1, \varphi_1, \dots, x_N, y_N, \varphi_N)^T$

Mass matrix: $\mathbf{M} = \text{diag}(m_1, m_1, I_1, \dots, m_N, m_N, I_N)$

Forces (here gravity only): $\mathbf{h} = (0, -m_1g, 0, \dots, 0, -m_Ng, 0)^T$

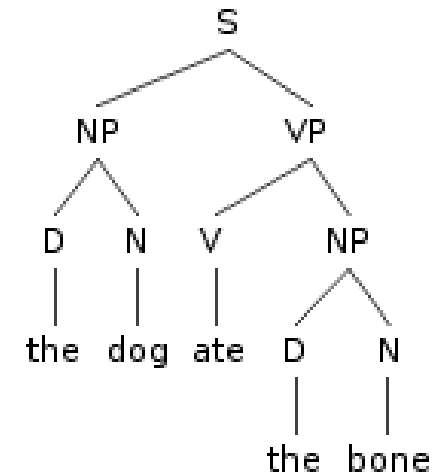
Vector of Constraints to model joints: Same as in Lecture 3

Robot Topology Design Synthesis



Origins of Transformational Grammar Rules in Linguistics

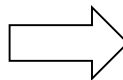
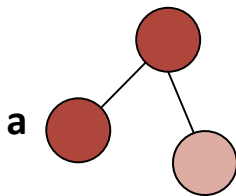
- A language is undefinable except for its grammar
 - proper ways to form valid statements
- Generative Grammars
 - Noam Chomsky - 1956
 - Rules that collectively define a language of feasible states
- A rule represents heuristic knowledge



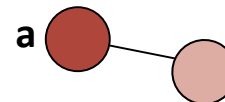
Graph Grammar(I)

- Graph rewriting system
- Rules used to change graph
 - Application conditions: Where the rule can be applied
 - Application procedure: What it does to the graph
- Rules represent heuristic knowledge

Left hand side of rule:
Pattern to find in graph

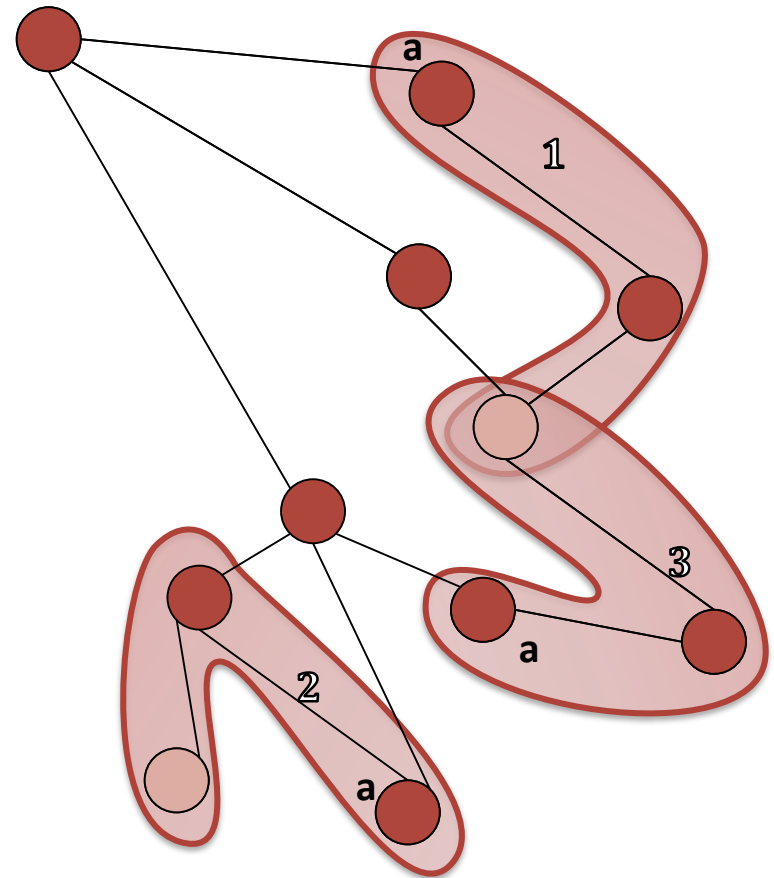
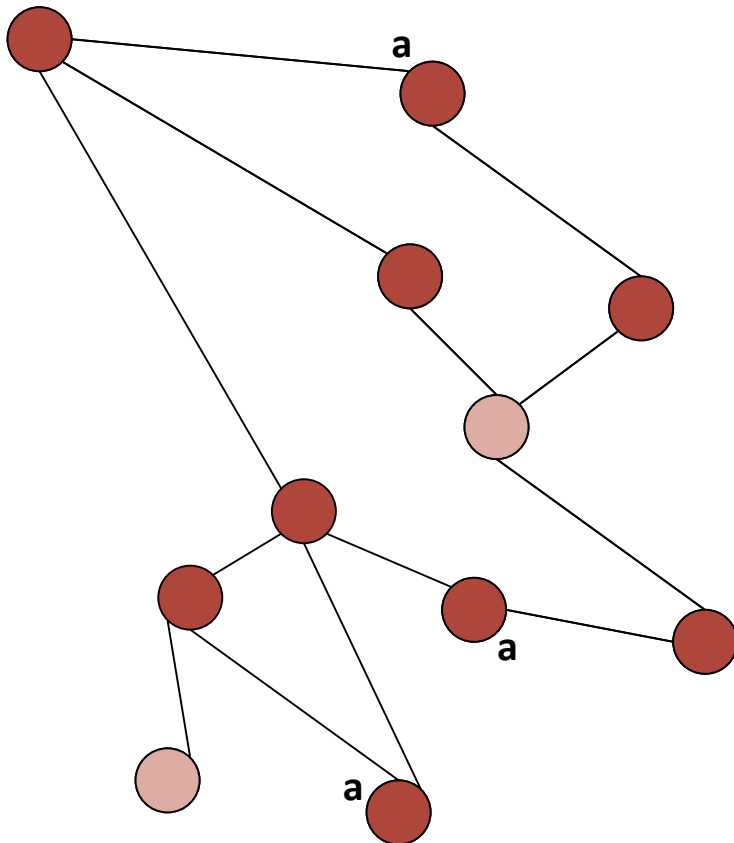
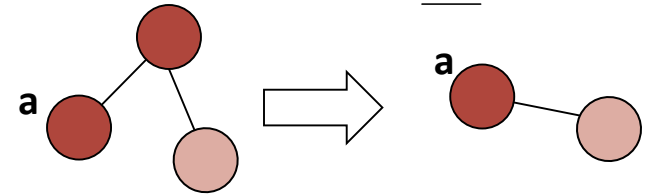


Right hand side of rule:
Replaces left hand side



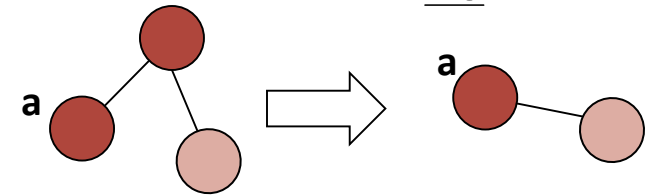
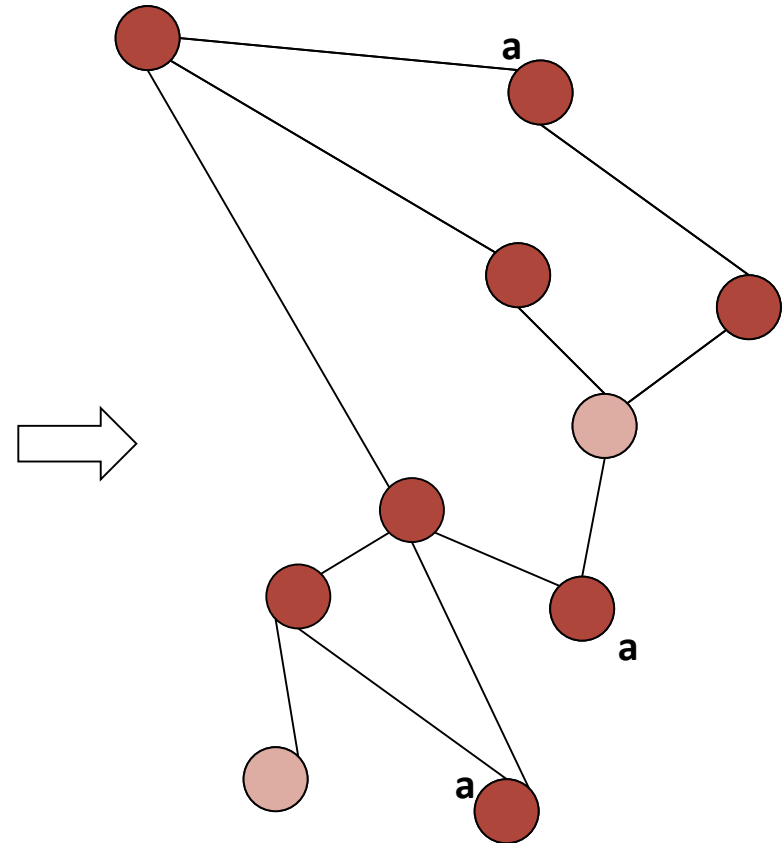
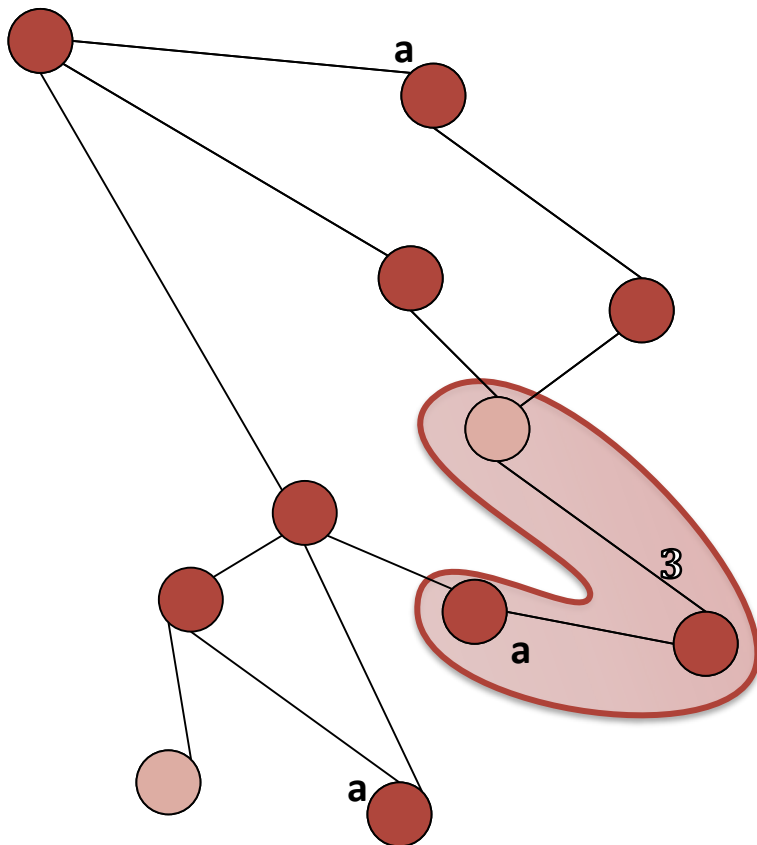
Graph Grammar(II)

Recognize left hand side of rule in graph



Graph Grammar(III)

Choose where to apply rule



Example: Gear Box Design

Topologic Rules

1 - Create a new Shaft



2 - Delete a Shaft



3 - Create a new Gear Pair



4 - Delete a Gear Pair



5 - Replace a Gear Pair



Parametric Rules

6 - Relocate Gear Pair along the Shafts



7 - Change Diameters of Gears



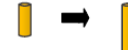
8 - Reposition a Shaft



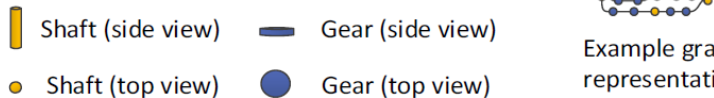
9 - Shorten a Shaft



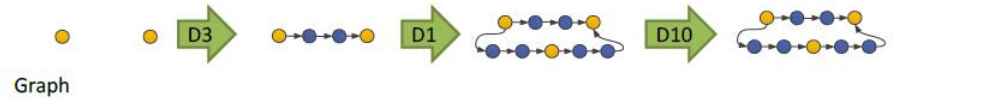
10 - Lengthen a Shaft



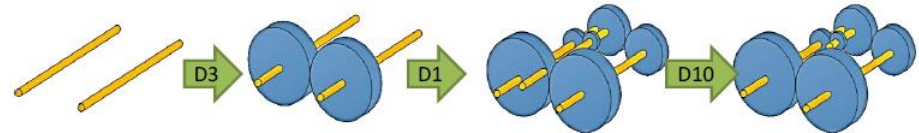
Legend



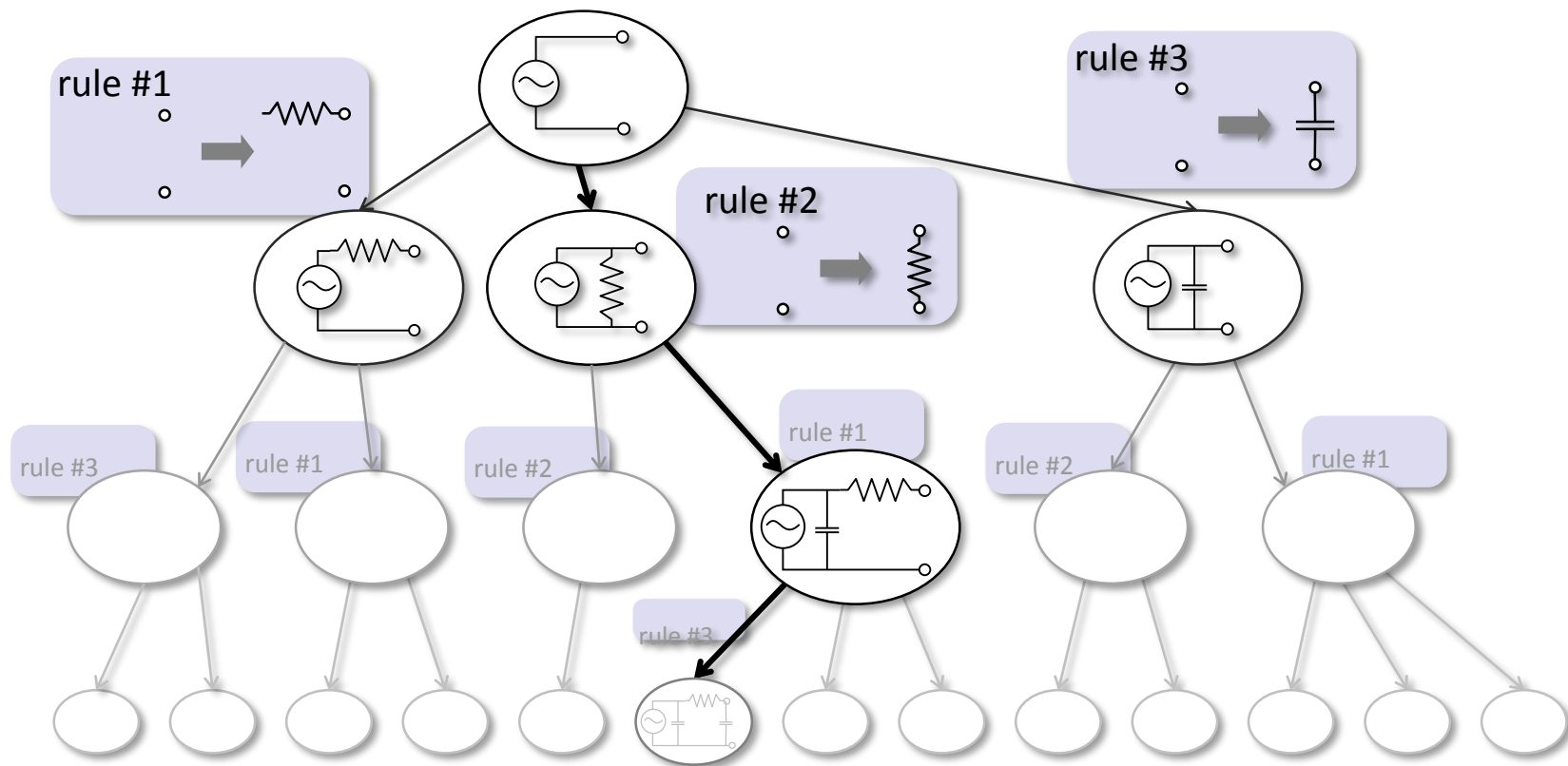
Change in graph



3D Representation

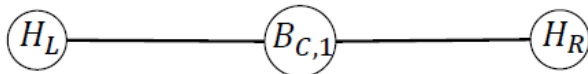


Example: Low-pass filters

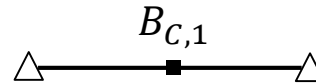


Design Rules for Passive Dynamic Systems (I)

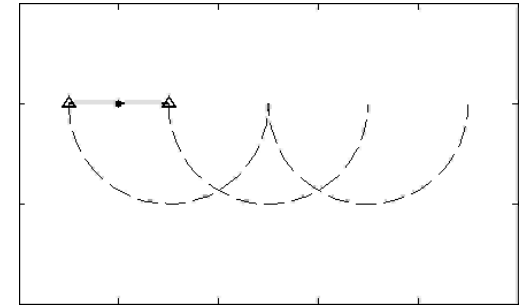
Graph Representation



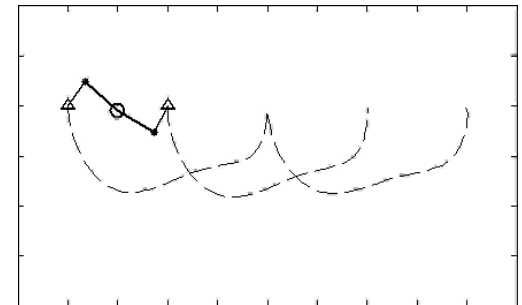
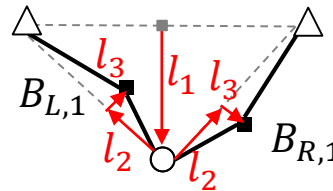
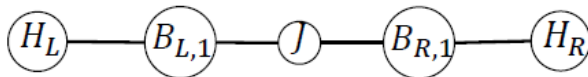
Multibody System



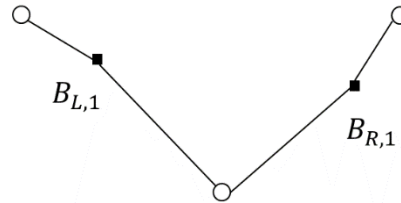
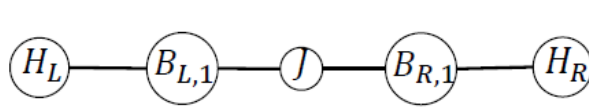
Simulation



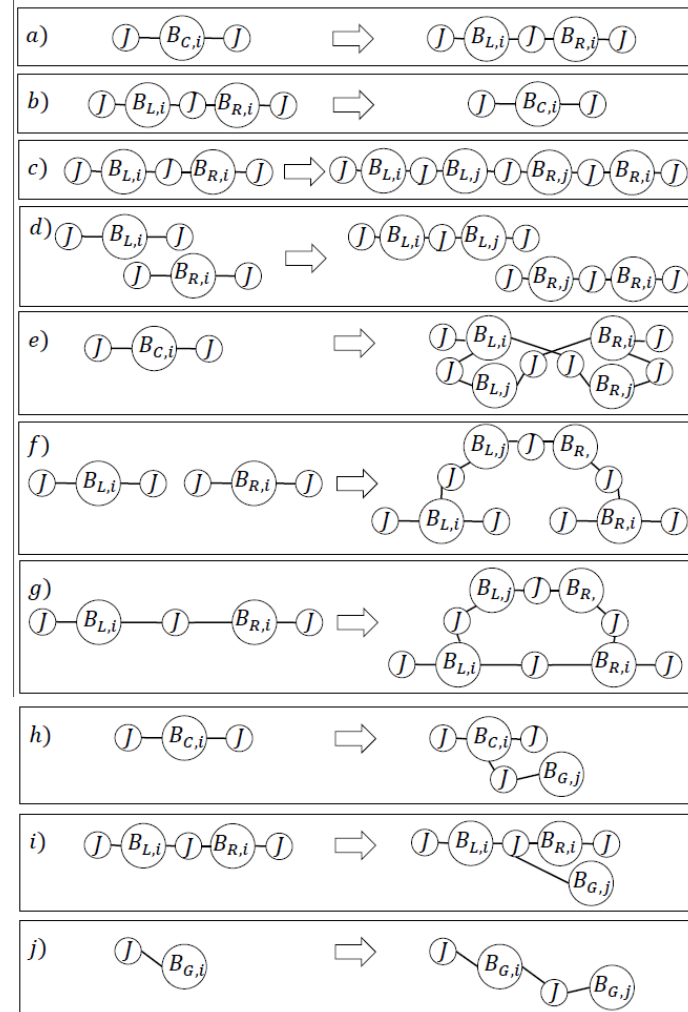
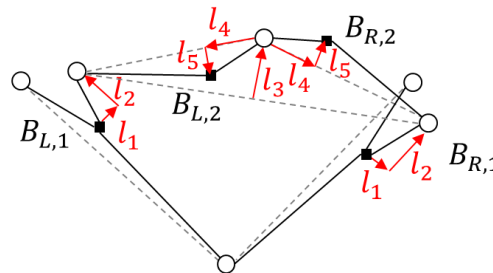
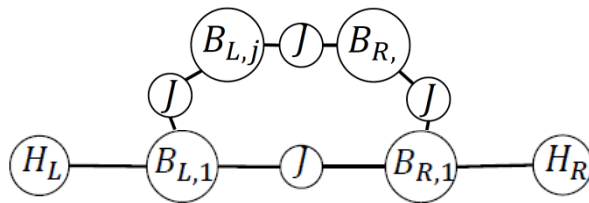
↓ Rule
ReplaceCBodyByLRBody



Design Rules for Passive Dynamic Systems (II)



Rule
AddLRBodyToLRBody



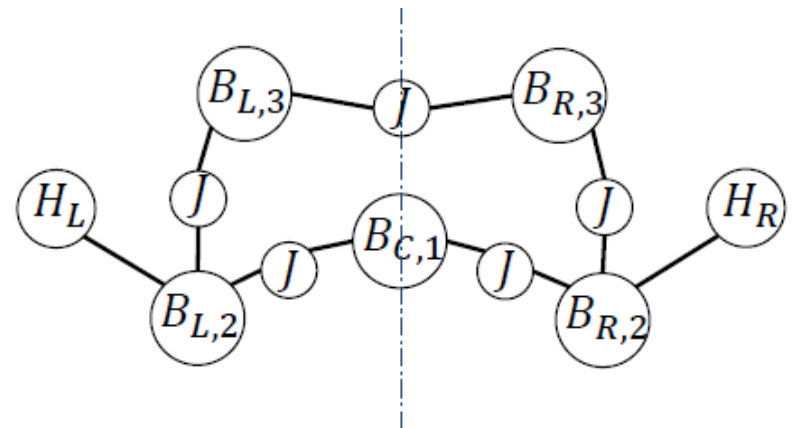
Symmetry for Brachiating (I)

Symmetry

- Is required for cyclic brachiating
- Similar as in walking between left and right leg

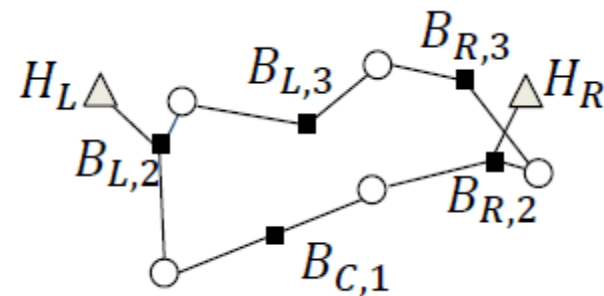
Symmetric Graph

- Rules generate symmetric configurations only
- Mirror symmetry



Symmetric Multibody System

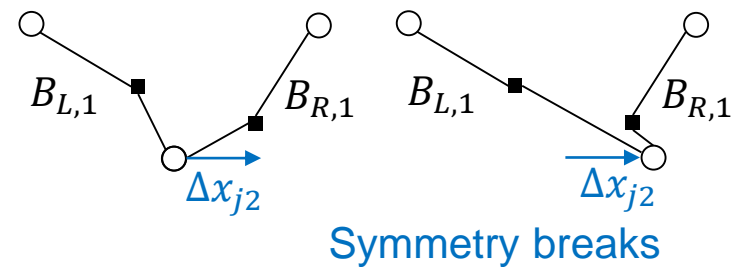
- Rules generate symmetric geometries only



Symmetry for Brachiating (II)

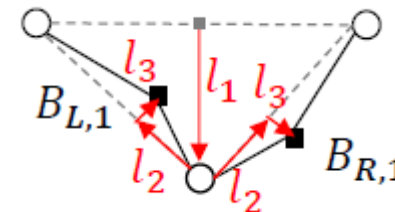
Arbitrary Parameterization

- Problem: Symmetry breaks

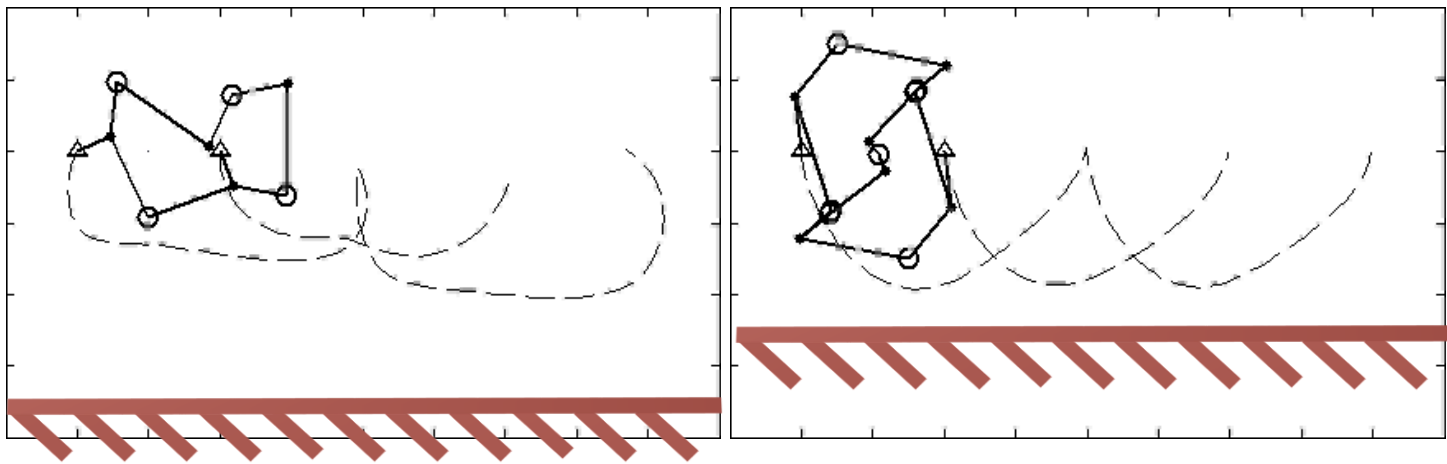


Symmetric Parameterization

- Symmetry is maintained when optimization variables are varied
- This is included in the design rules



Evaluation Criteria



Cyclic Locomotion

- Number of successful swings
- Difference in states and hand position after first and last swing

$$f_{4a} = -n_{sw}$$

$$f_{4b} = \Delta_{pos}(t_1)a_1 + \Delta_{vel}(t_1)a_2 + \Delta_{hand}(t_1)a_3 + \Delta_{hand}(t_{end})a_4$$

Space Requirement

- Lowest coordinate swept during the whole motion

$$f_5 = -y_{min}$$

Complexity

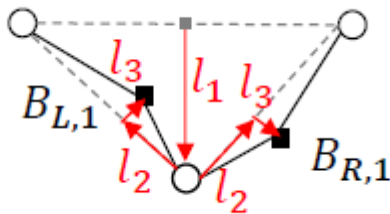
- Measured by the number of bodies

$$f_6 = -n$$

Synthesis and Optimization

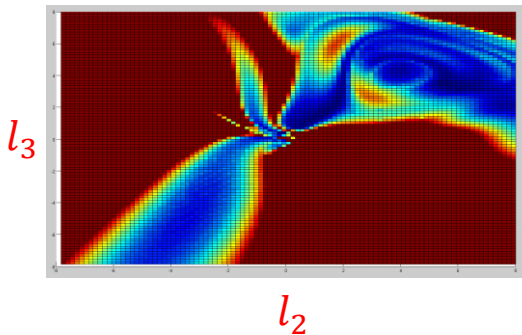
Parametric Optimization

- For each topology generated
- Multi-objective genetic algorithm (pop size: 200, generations: 80) From Matlab toolbox
- Highly non-linear, non-convex multi-modal optimization landscape



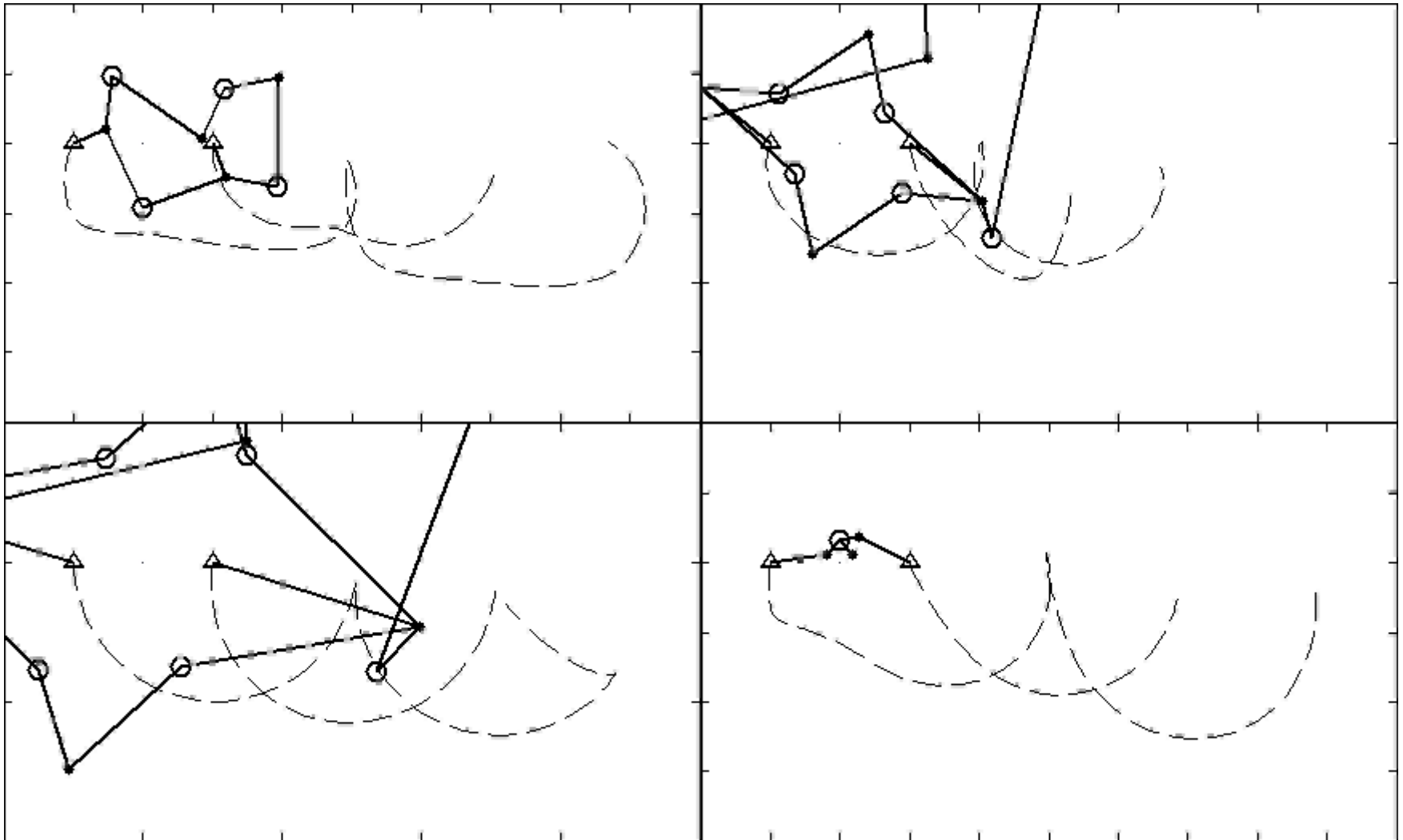
Topological Synthesis

- Multi-objective burst algorithm (burst length: 3, max iterations: 500)



Cyclic locomotion:
blue: good performance
red: poor performance

Intermediate Solutions after some Generations



Results

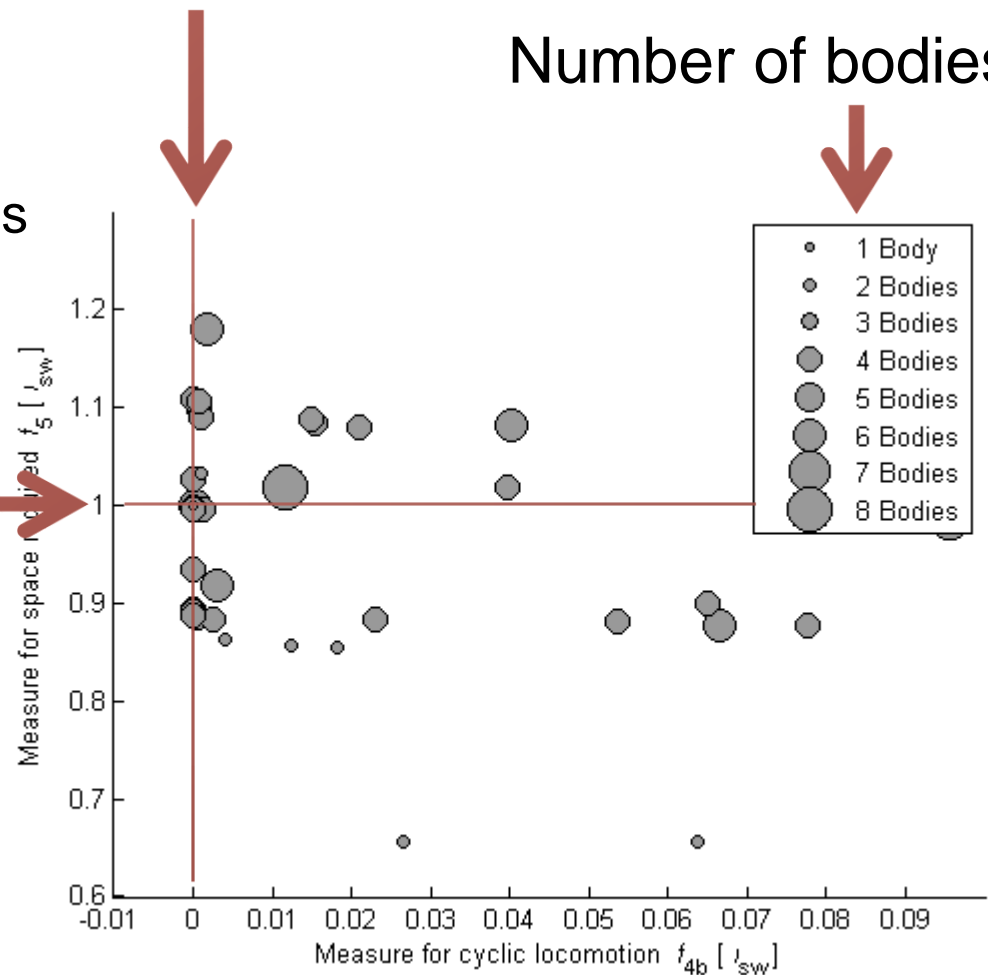
Evaluation Plot

- Final populations of eight different topologies
- All do three successful swings
- 3 Objectives

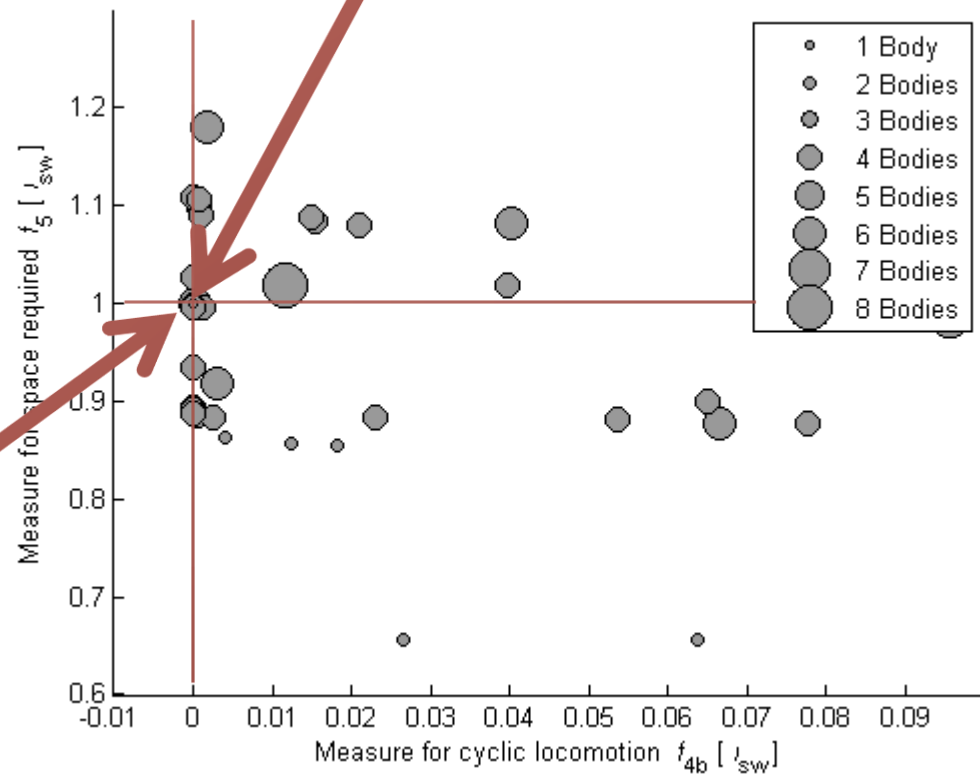
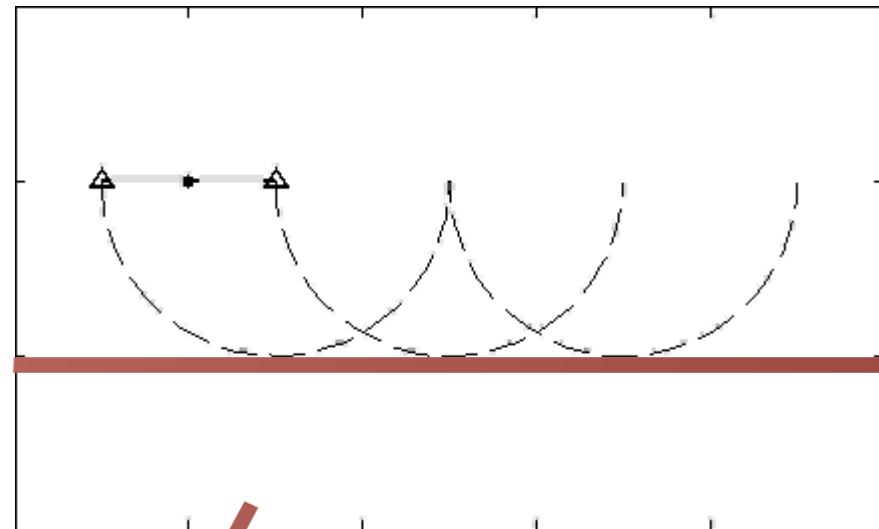
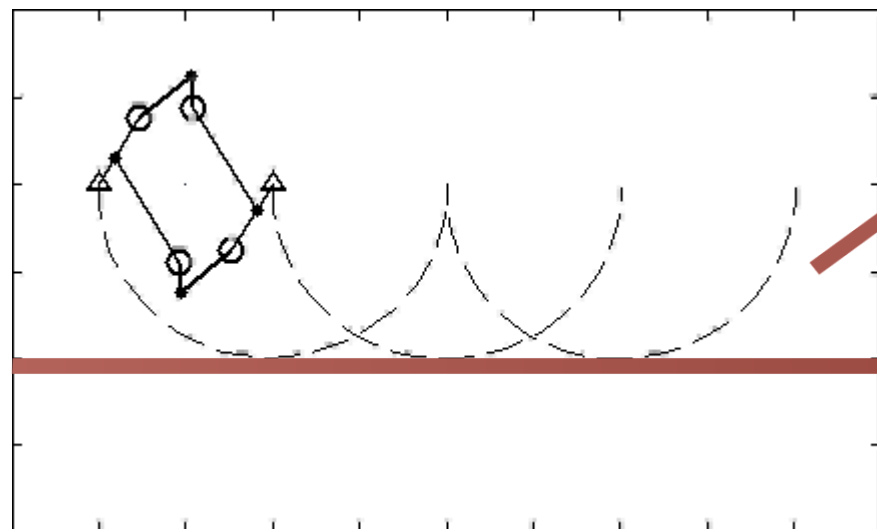
Space requirement
of single pendulum

Ideal cyclic locomotion

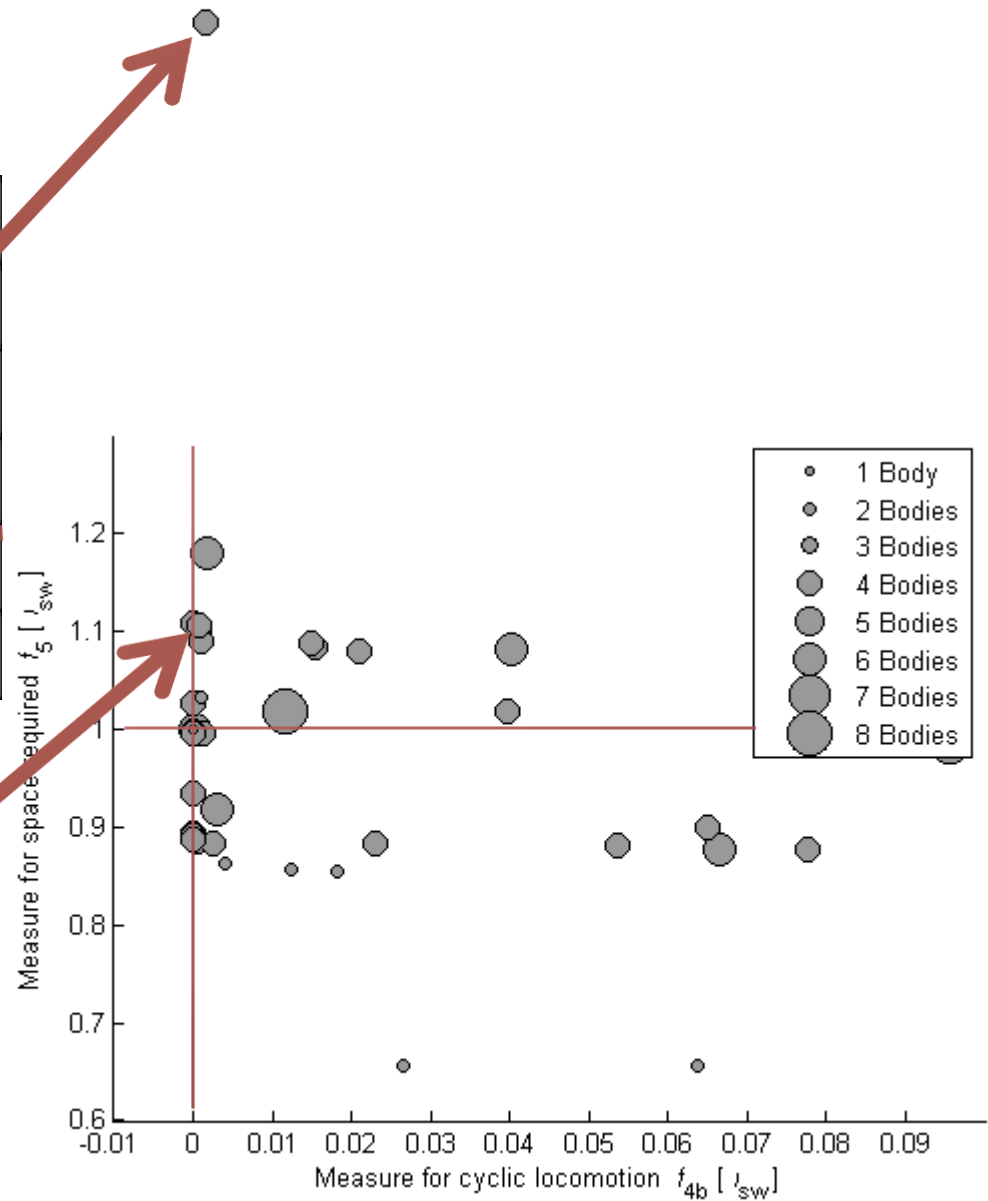
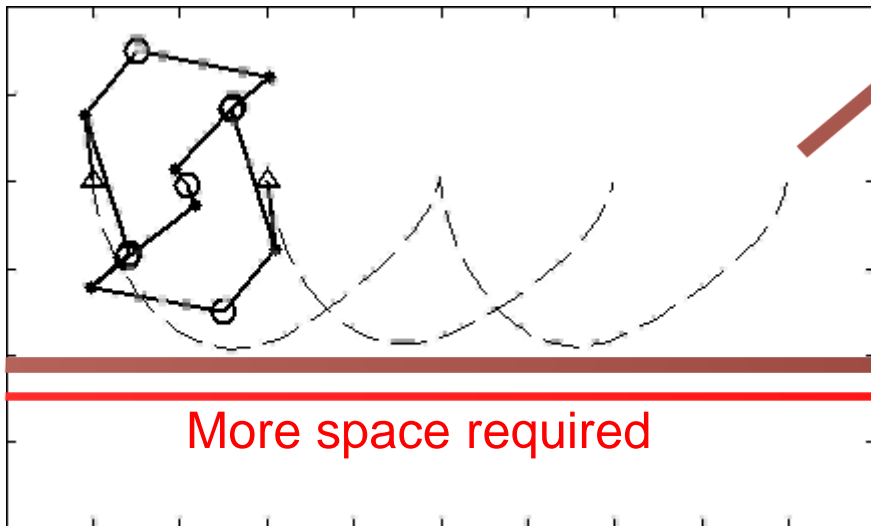
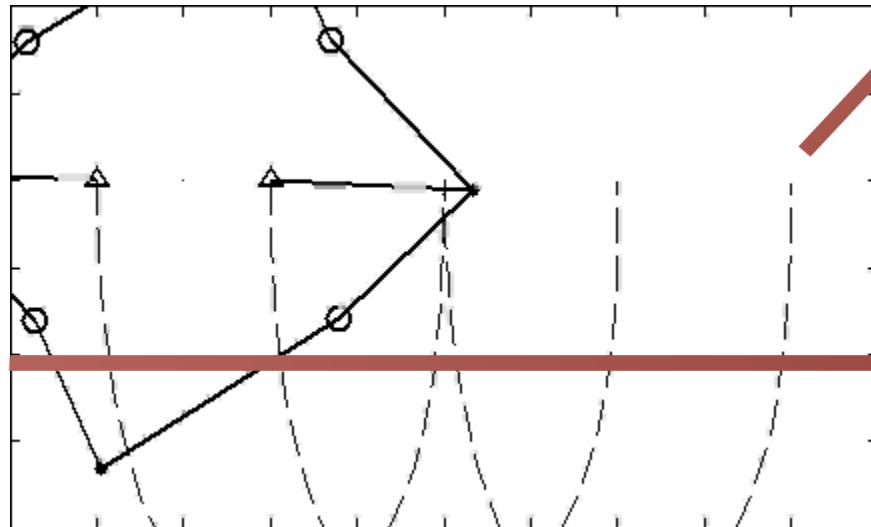
Number of bodies



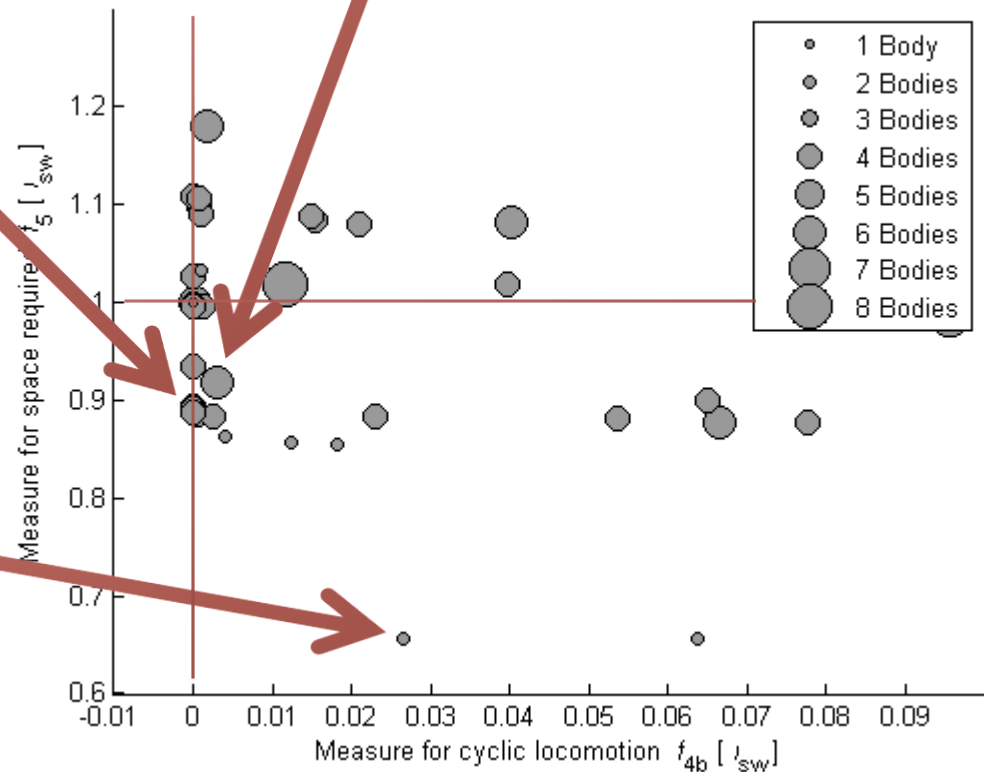
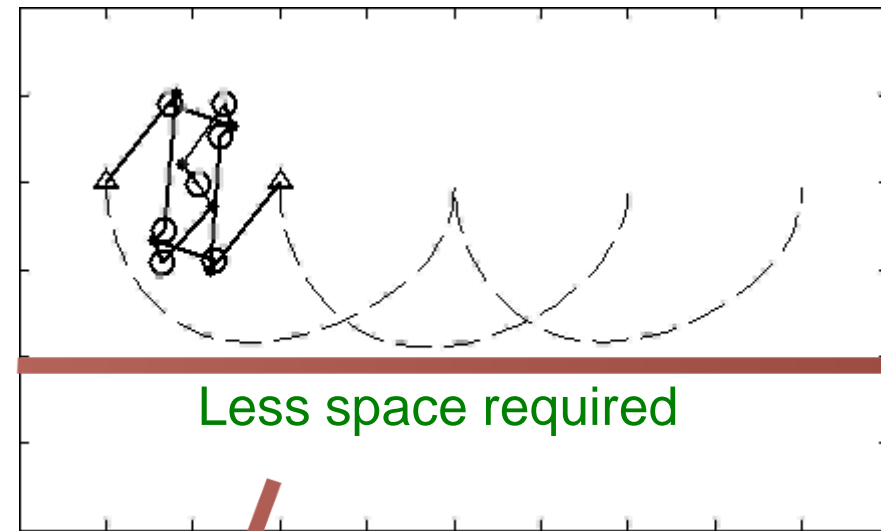
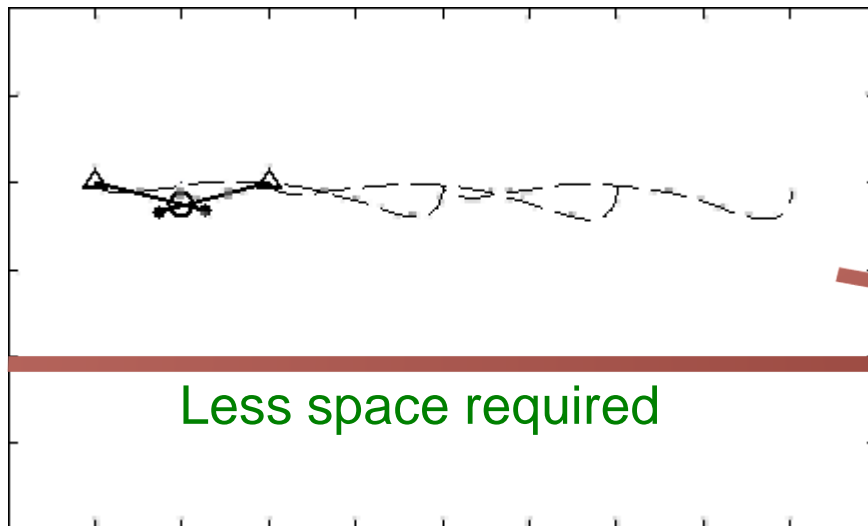
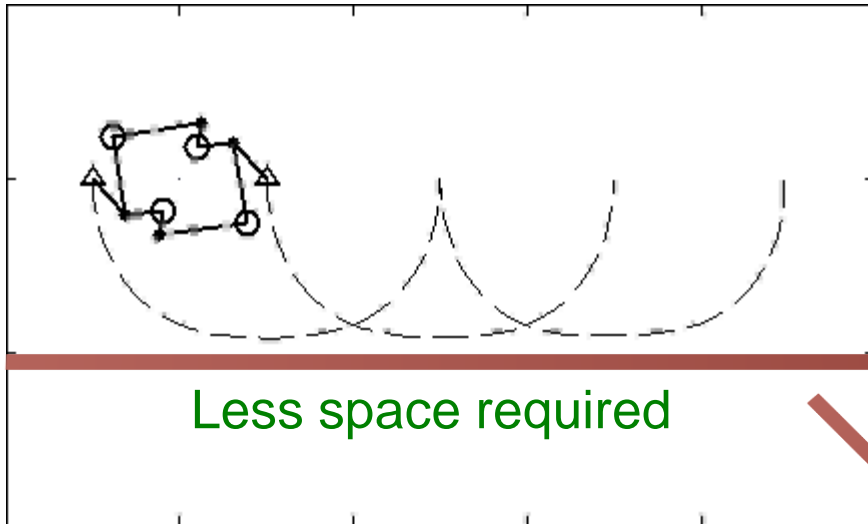
Results



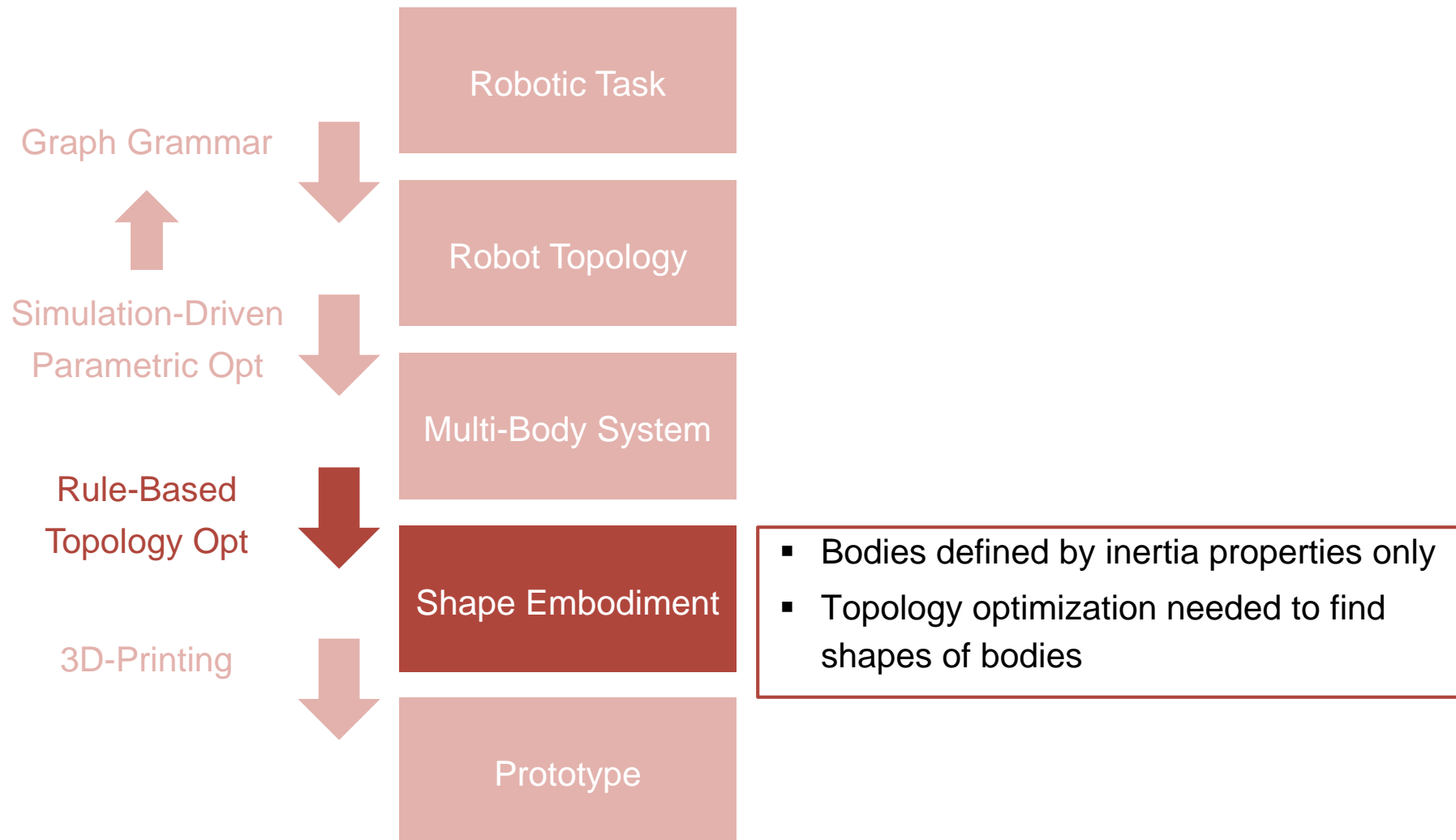
Results



Results

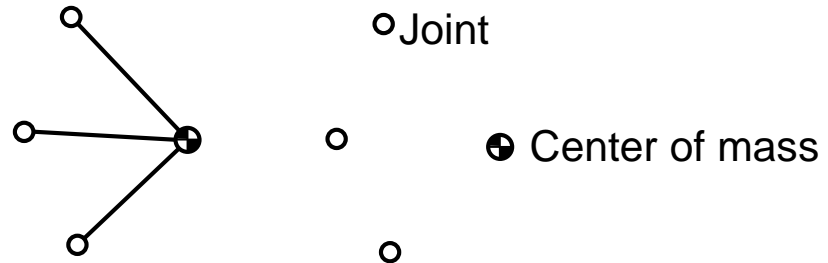
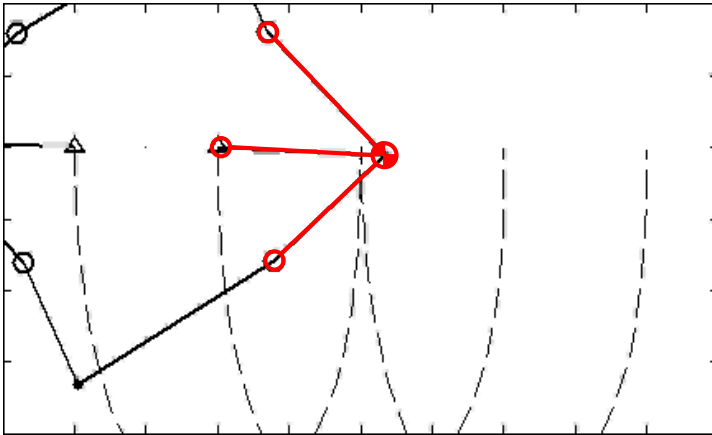


Shape Embodiment Design



Automated Shape Design for Multi-Body Systems

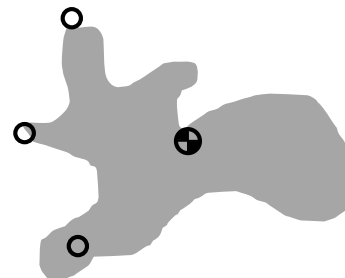
Multi-body system representation



Dynamic properties:
[Mass, moment of inertia,
center of mass]

Find shape

- Matching dynamic properties
- Connecting all elements
- Avoiding collisions

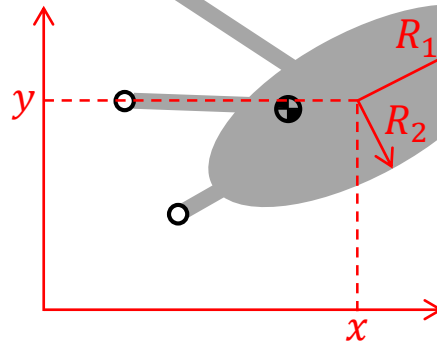


Assemble Geometric Primitives

Find shape with given dynamic properties

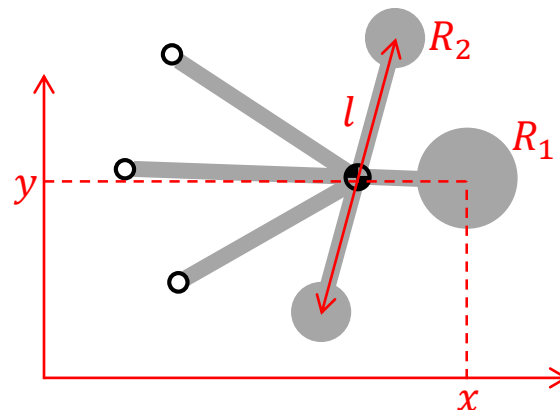
Ellipse

- 5 variables: x, y, R_1, R_2, α
- Sometimes no solution found
- Compact

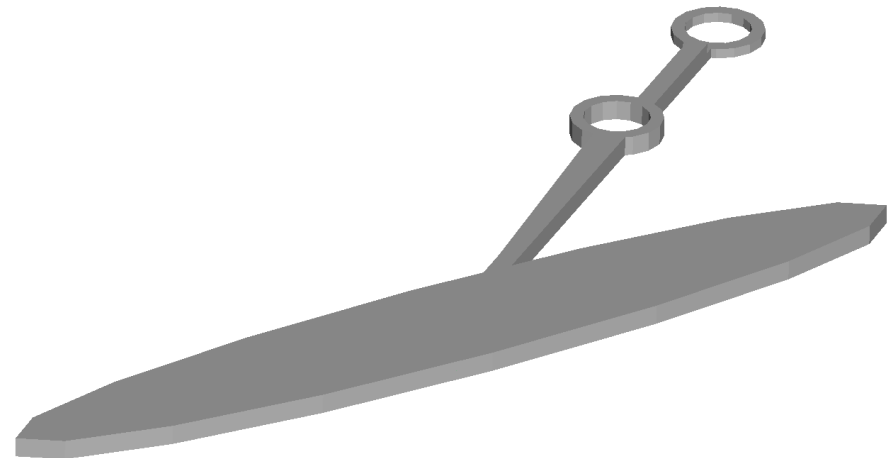
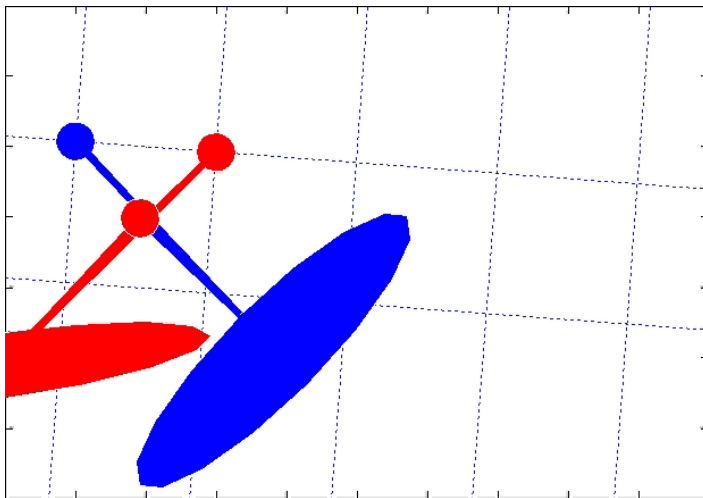
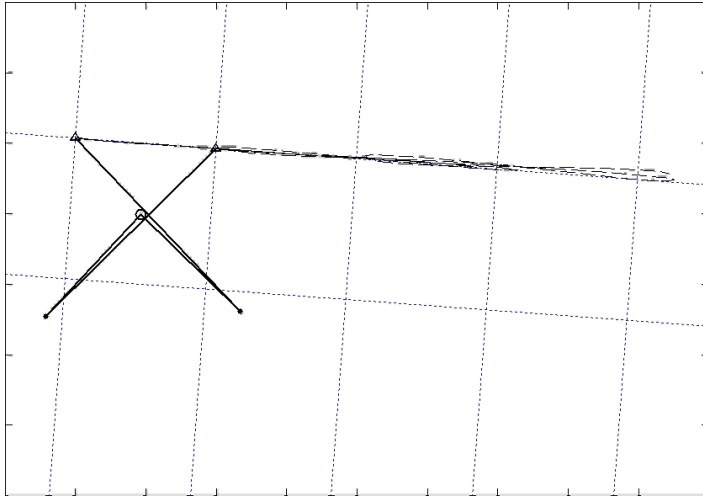


Three Circles

- 6 variables: $x, y, R_1, R_2, \alpha, l$
- Mass and Moment of inertia change more independently
- Uses more space



Assemble Geometric Primitives



Finite Element Design Space

ρ_i Density of element i /
Material per 2D element i

m_0, I_0, c_{x0}, c_{y0} Desired dynamic properties

Feasibility/Satisfiability Problem:

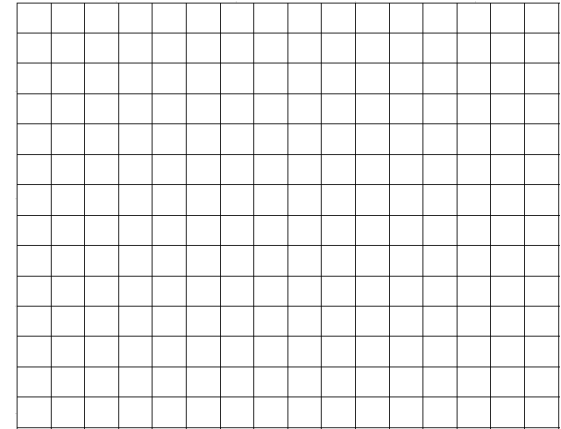
$$\mathbf{m}^T \boldsymbol{\rho} = m_0$$

$$\mathbf{I}^T \boldsymbol{\rho} = I_0$$

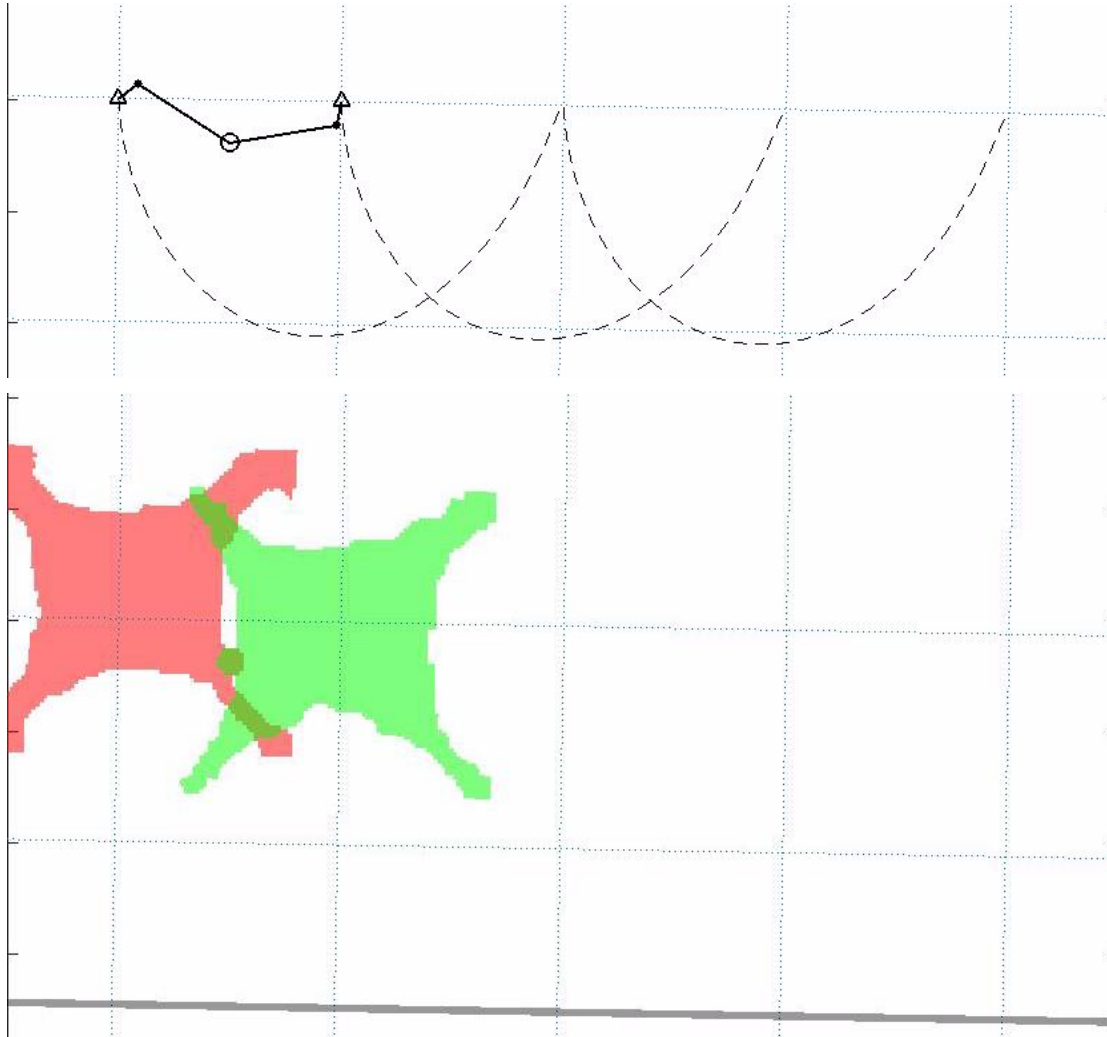
$$\frac{\mathbf{c}_x^T \boldsymbol{\rho}}{\mathbf{m}^T \boldsymbol{\rho}} = c_{x0}$$

$$\frac{\mathbf{c}_y^T \boldsymbol{\rho}}{\mathbf{m}^T \boldsymbol{\rho}} = c_{y0}$$

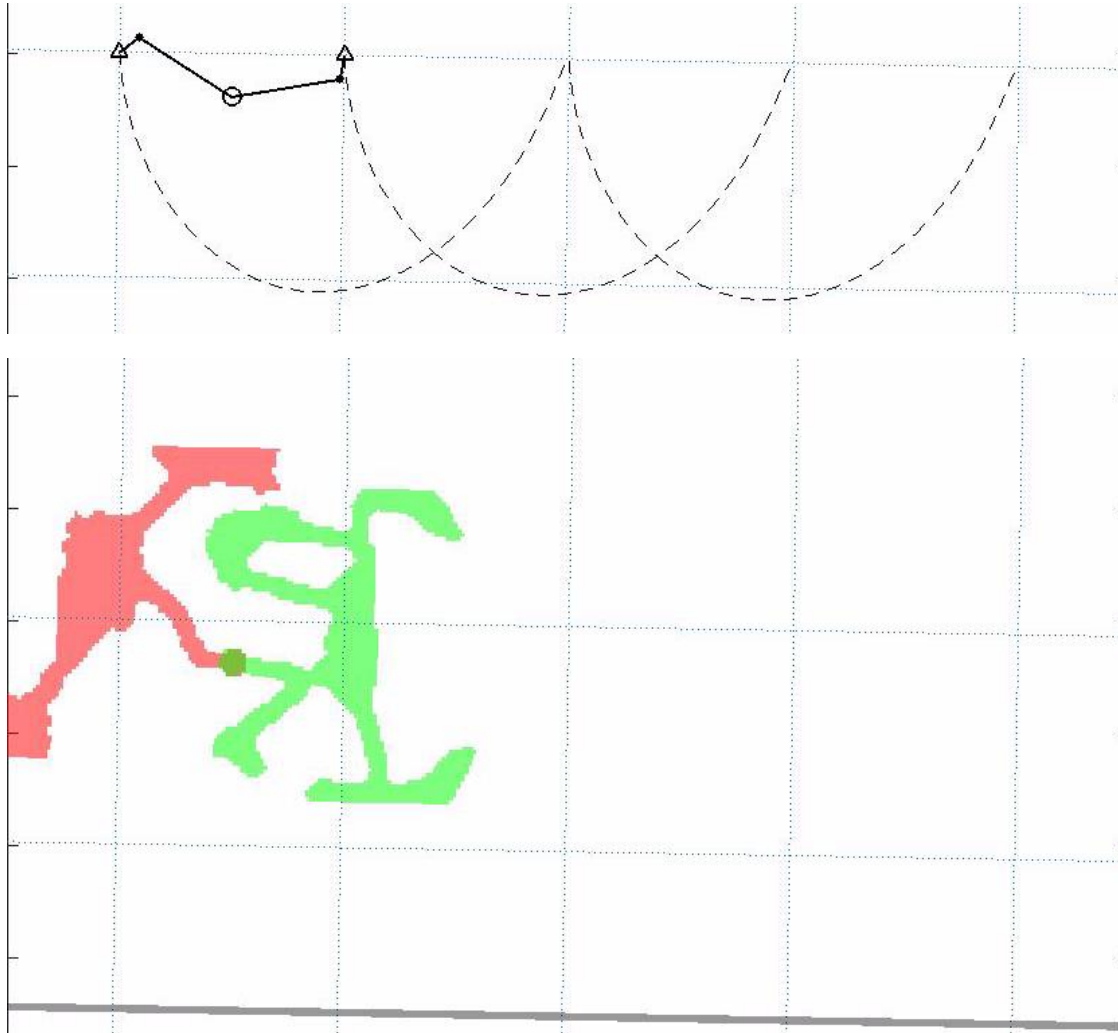
$$0 \leq \rho_{min} \leq \rho_e \leq \rho_{max}$$



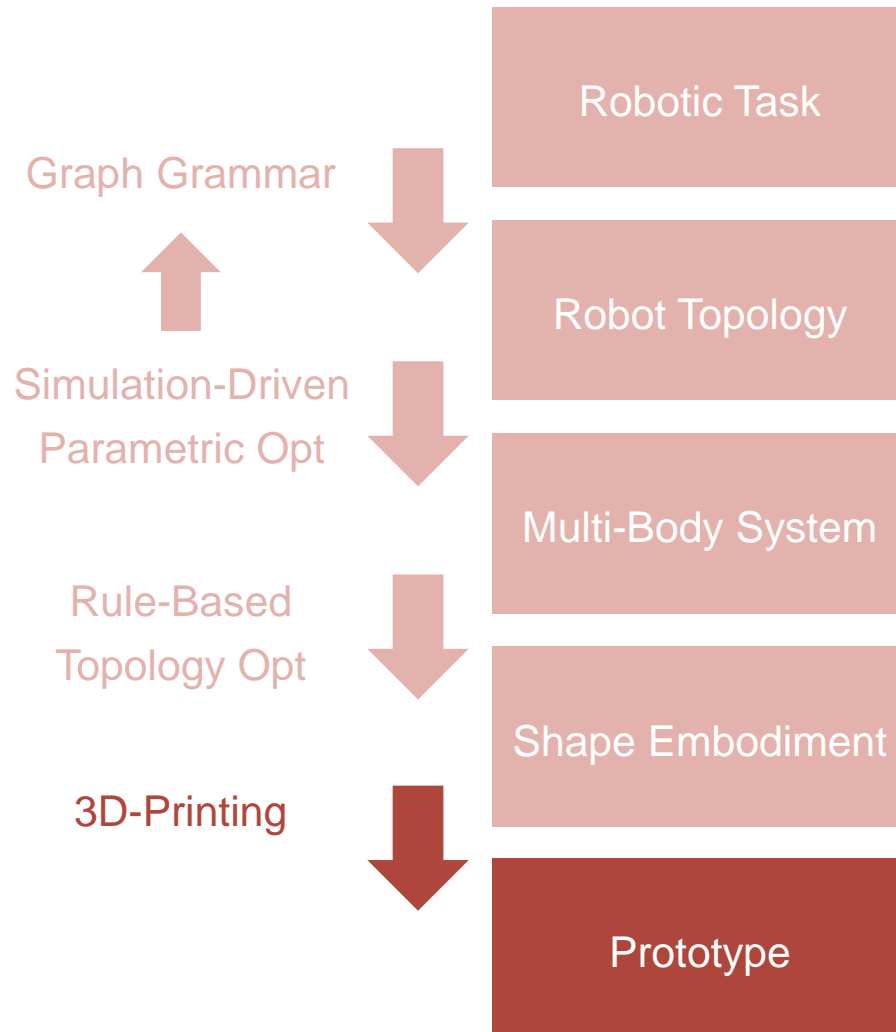
Finite Element Design Space



Finite Element Design Space



Fabrication



- Additive manufacturing works well for complex shapes
- Ball bearings for low friction



Experiment and Optimization based Design of a Passive Walking Robot, Fabio Modica, 2016, EDAC master thesis

Measure static/dynamic friction of bearing

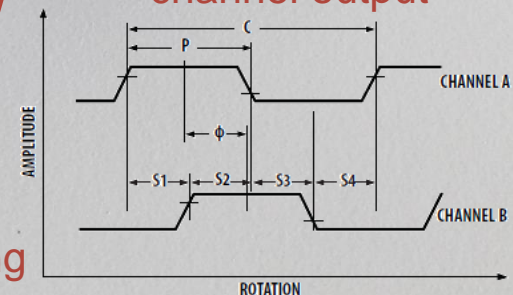
Arduino Board

Codewheel with 1024 counts per revolution

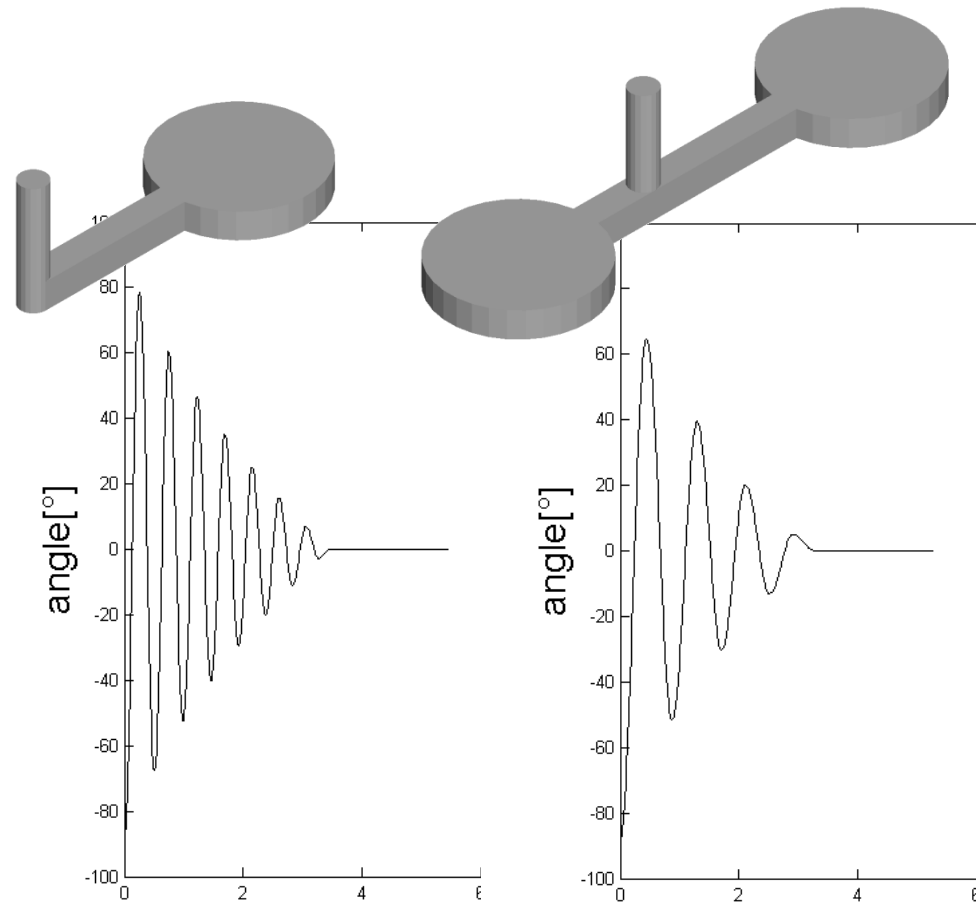
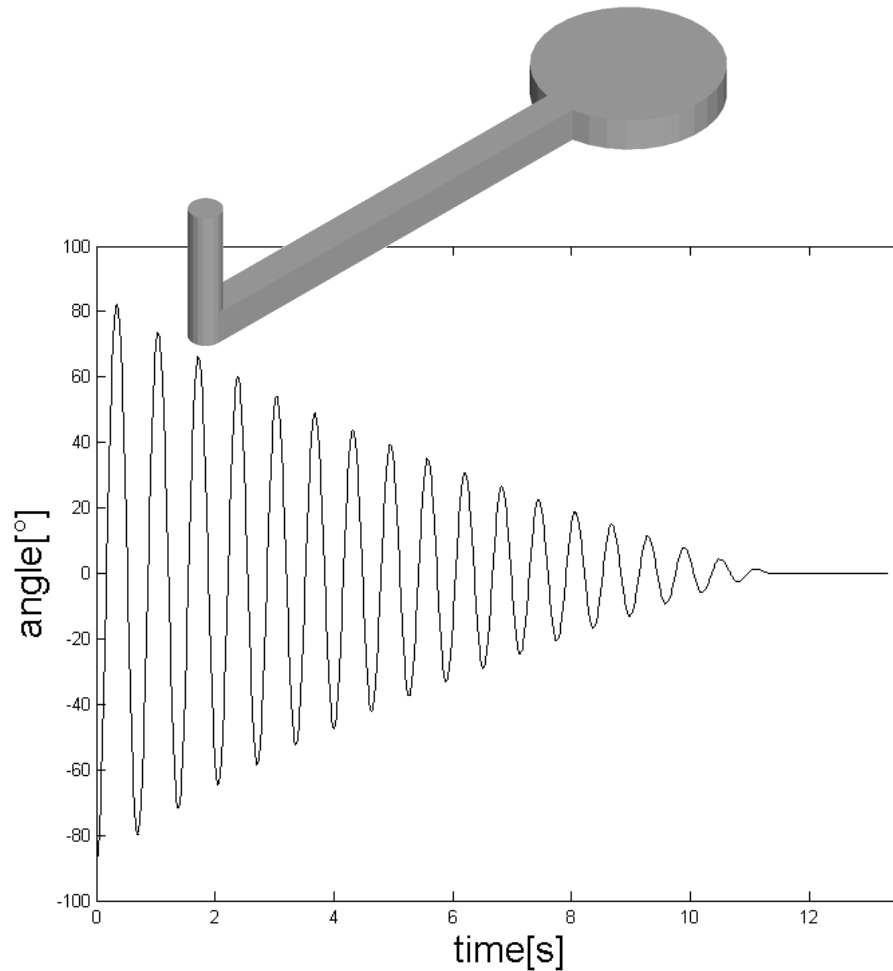
Three pendulums with different dynamic properties

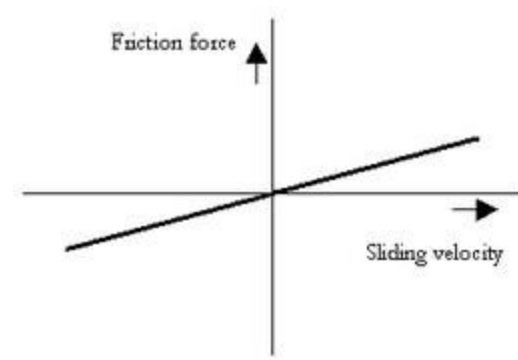
Optical incremental encoder with two channel output

Ball bearing



Measurement results

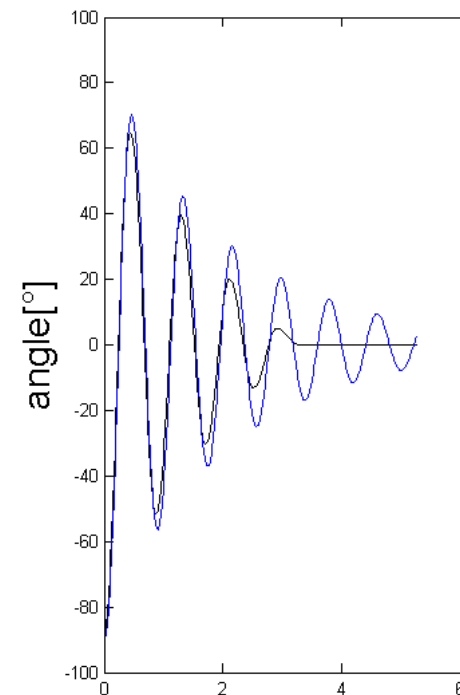
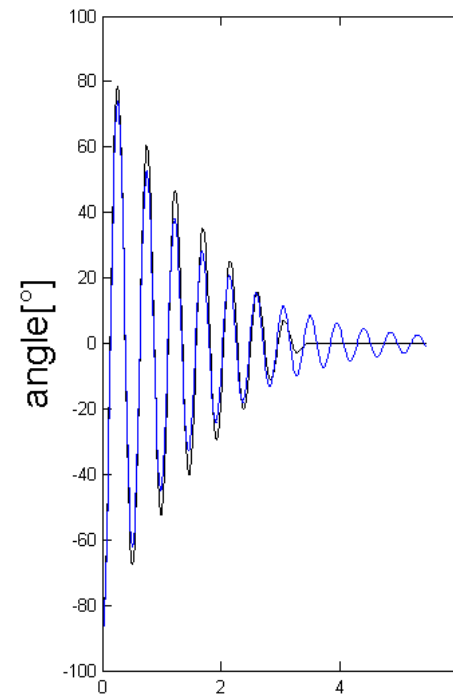
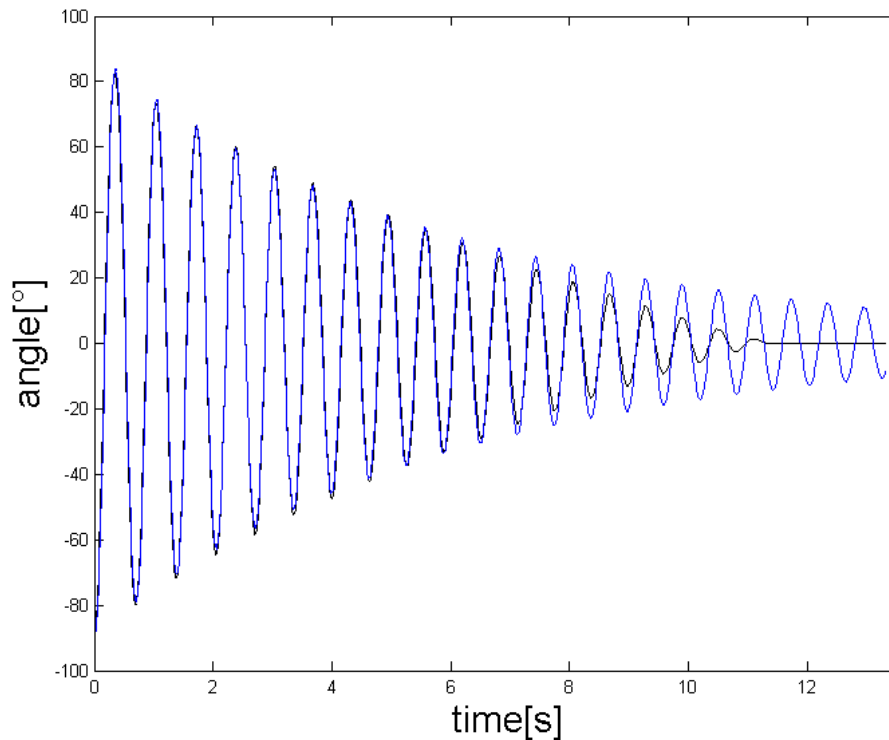




Fit Measurement to Simulation Model

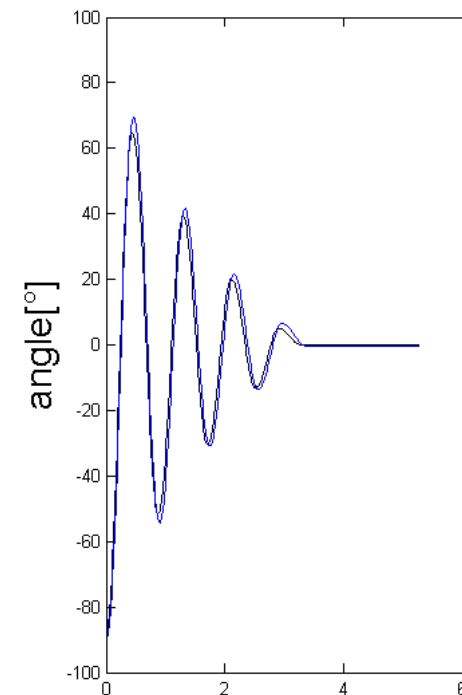
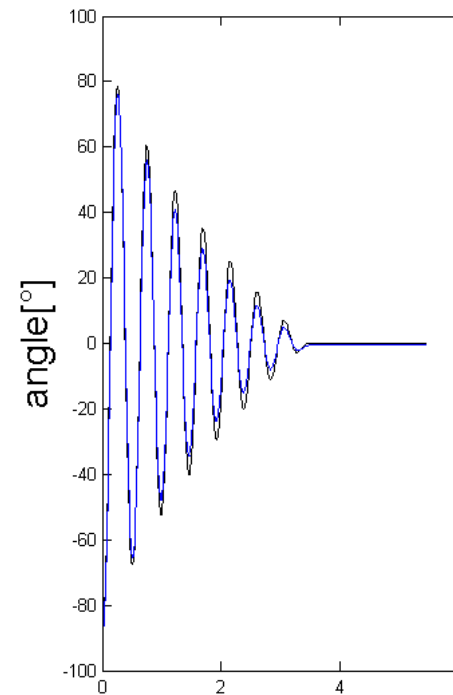
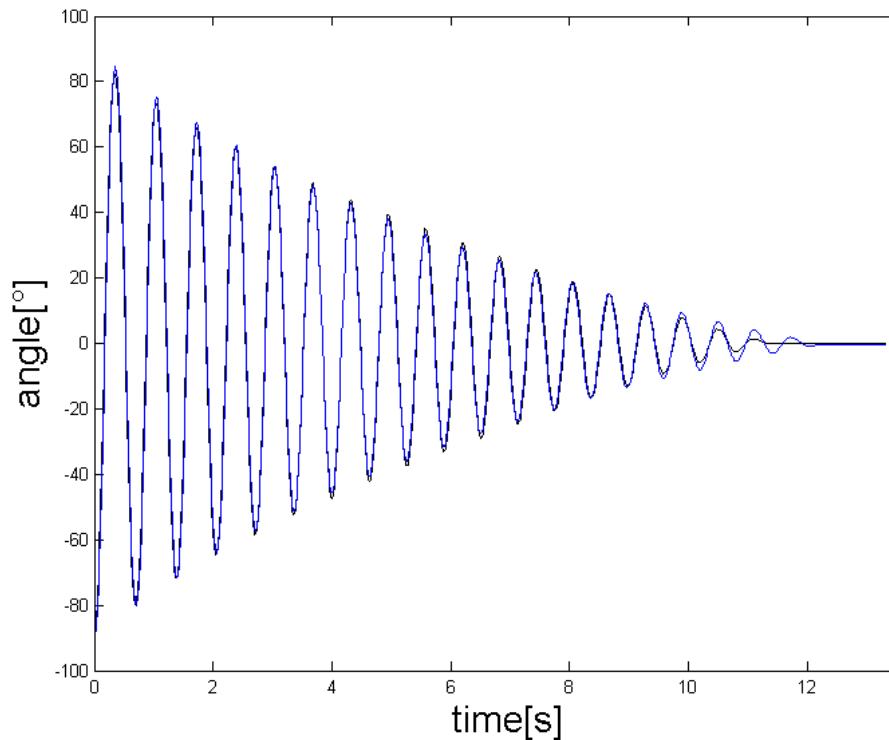
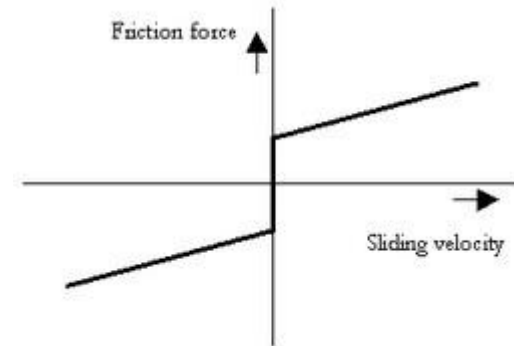
$$\ddot{\phi} I = -mgl \sin(\phi) - d_F \dot{\phi}$$

Friction Torque velocity proportional (viscous friction):
Standard in robotics, good properties of ODE and
control problem



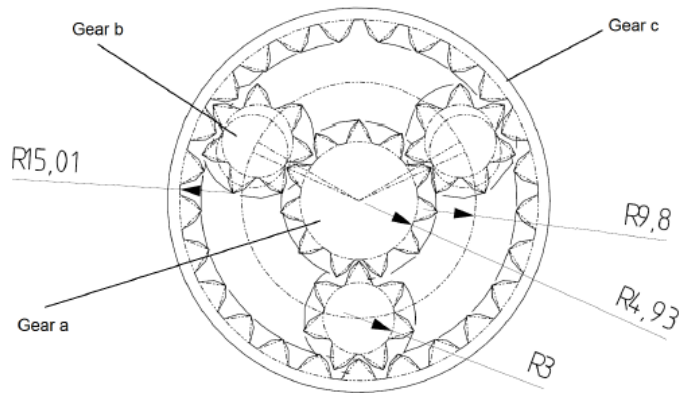
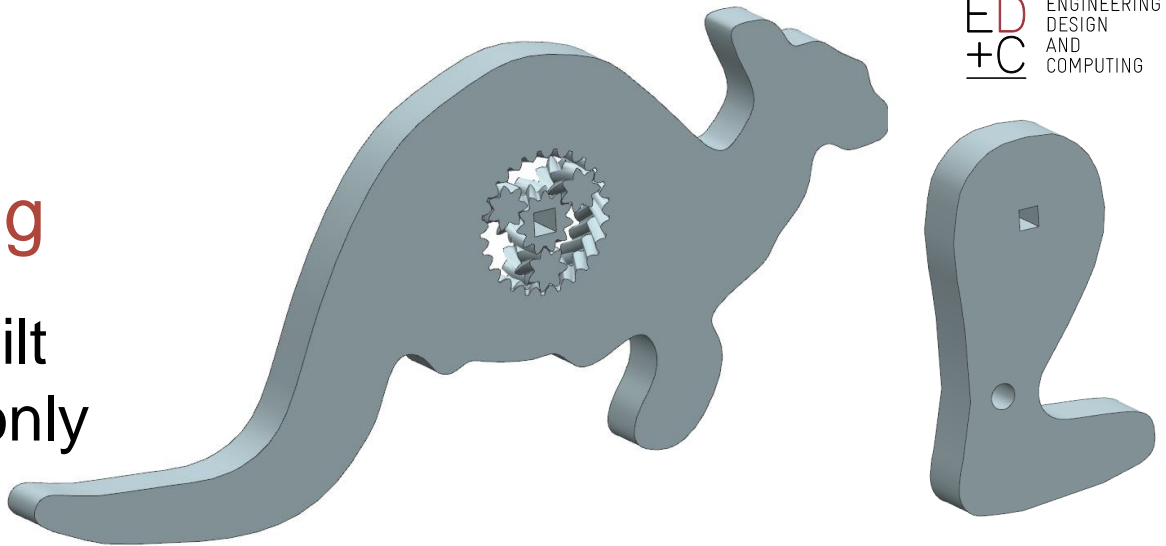
Fit Measurement to Simulation Model

$$\ddot{\varphi} I = -mgl \sin(\varphi) - T_F \quad \text{Combination of viscous friction and coulomb friction}$$

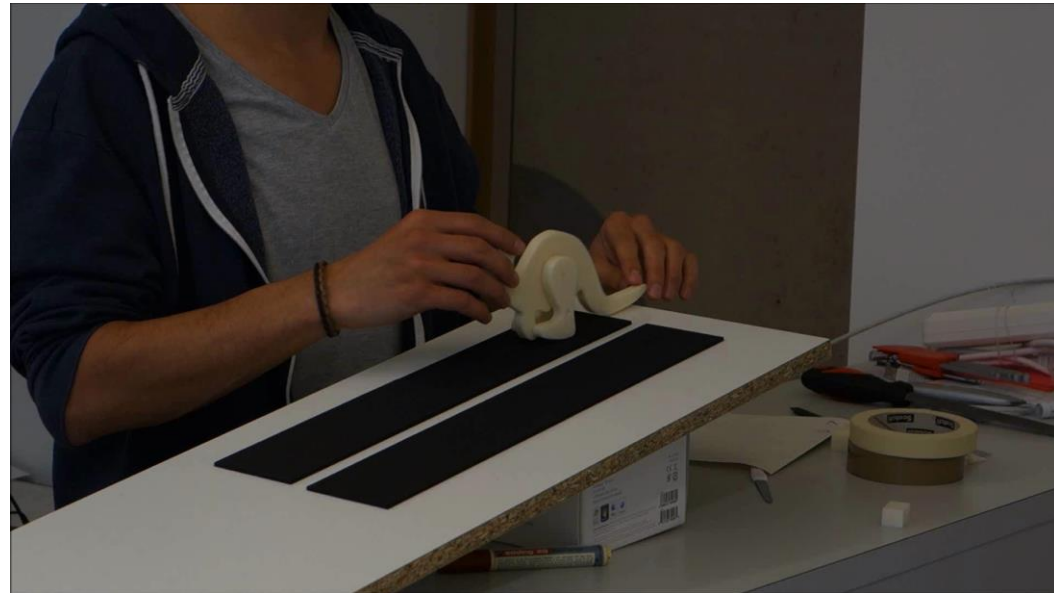


3D-Printed Bearing

- Passive walker built using FDM parts only
- Printed in one job

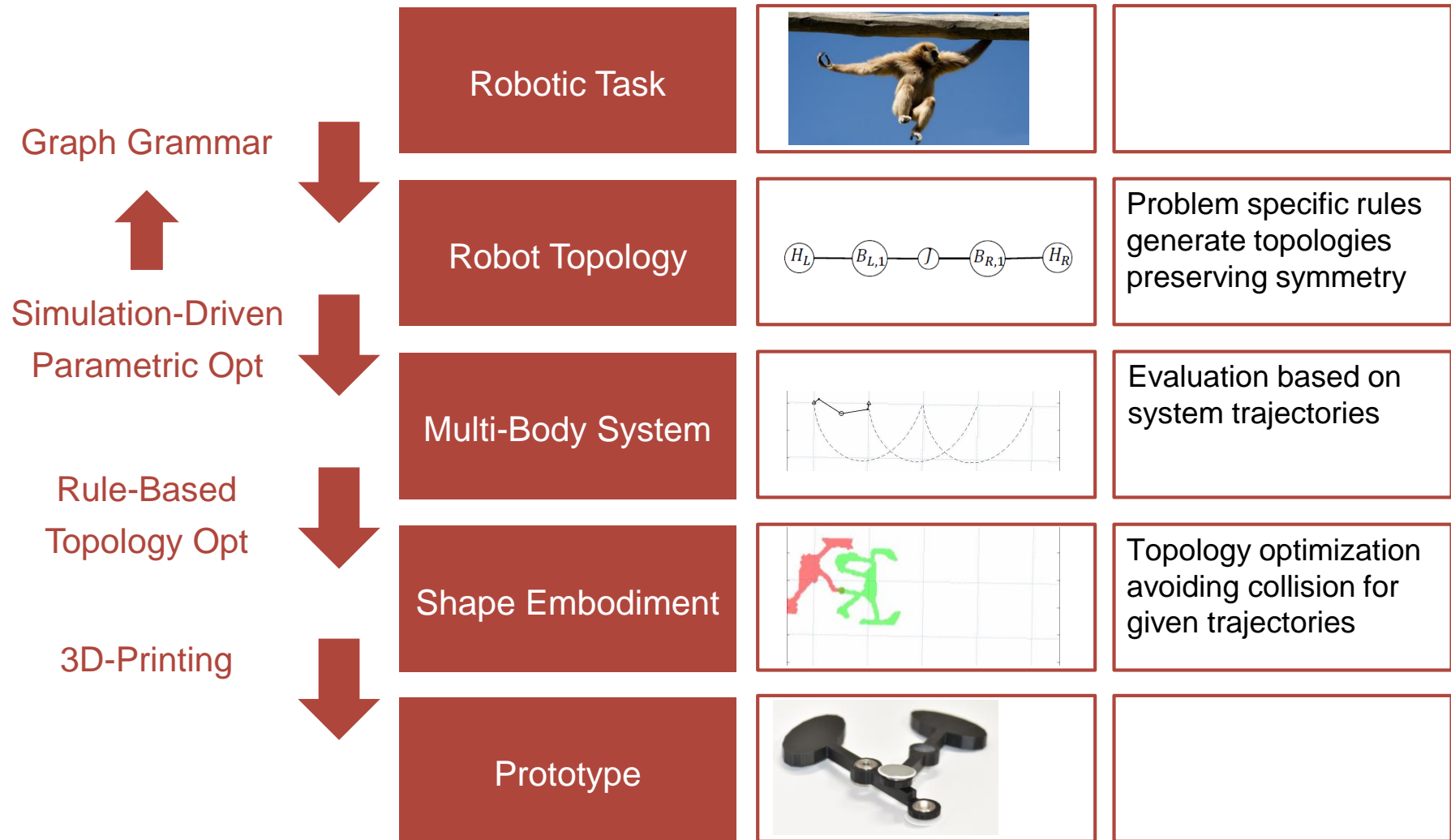


- Planetary gear bearing with clearance adapted to our FDM machine



- Very robust gait

CDS of Passive Dynamic Systems - Overview



Future Work

- Evaluation
 - Sensitivity analysis
- Additional joint types, friction, springs, ...
- Other robotic tasks
- Prototyping
- Synthesis and optimization
 - Different strategies

